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Permeable Reactive Treatment (PeRT) Wall

# Characterization Report

September 1998



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September 1998

Prepared for
U.S. Department of Energy
Albuquerque Operations Office
Grand Junction Office

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## 1.0 Introduction

This report presents and discusses results of a subsurface investigation conducted in May and June 1998 to support the design and construction phases of the Monticello Permeable Reactive Treatment (PeRT) project, Monticello, Utah. The objective of this investigation was to determine bedrock depths, water table elevations, subsurface lithology, and uranium concentrations in ground water, in the immediate vicinity of the proposed PeRT wall. Relevant data obtained during the Monticello Mill Tailings Site (MMTS), Operable Unit (OU) III remedial investigation have also been incorporated.

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## 2.0 General Setting

The project area is located in the central portion of a valley through which a small perennial stream (Montezuma Creek) flows. The creek flows west to east at rates typically about 1 cubic foot per second or less, although significantly higher flows occur during spring runoff and storms. The creek banks are steep in the project area and rise about 10 ft above the stream stage. On the north side of the creek, the valley floor is relatively flat in width (north-south) for approximately 250 ft. North of the flat area, the ground surface rises sharply about 25 feet (ft) above the valley floor, and then becomes moderately sloped over the next several-hundred feet. South of the creek, the ground surface rises gradually over a distance of 200 to 300 ft. On both sides of the creek, but beyond the immediate area of interest, the valley is bounded by steep bedrock hillslopes.

Within the central portion of the valley, 10 to 20 ft of unconsolidated deposits overlie bedrock. The unconsolidated materials consist of a layer of fine, sandy silt that overlies approximately 5 to 8 ft of alluvial sand, gravel, and cobbles. Ground water is present in the alluvial materials and forms a shallow and relatively narrow water table aquifer. The direction of ground-water flow is regionally from west to east, parallel to the trend of the valley, but varies considerably on a local scale. In the project area, the alluvial aquifer is underlain by about 35 ft of interbedded mudstone, siltstone, sandstone, and occasional coal seams of the Dakota Sandstone Formation. The bedrock topography generally mimics that of the ground surface. Bedrock in the project area strikes approximately due north and dips about 1 degree to the east.

The Dakota Sandstone Formation is an aquitard that separates the alluvial aquifer from the underlying sandstone aquifer within the Burro Canyon Formation. The PeRT wall will be constructed in the alluvial aquifer, which is contaminated by mill tailings-related constituents. The Burro Canyon sandstone aquifer is not contaminated.

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#### 3.0 Field Program

Subsurface conditions were investigated for the PeRT project during May and June 1998 at the 19 locations shown in Figure 3–1. At each location, a 2-in o.d. core sampler was advanced using a hydraulically powered direct push/percussion probe rig (Geoprobe® Systems, Model 4200). Manufacturer specifications indicate a hydraulic pressure of 2000 psi, 16,000 lb of down pressure, and percussion rate of 30 Hz for the model used. Also shown in Figure 3–1 is the location of the PeRT wall as currently proposed and the locations of other previously installed boreholes and monitoring wells.

Each probe hole completed during the 1998 investigation was extended into bedrock, however continuous core sampling of the unconsolidated deposits was not performed and therefore a complete record of subsurface lithology and individual bed thickness was not obtained. The core sampling was conducted to complement the detailed lithologic data obtained during 1992 (see below) and to provide additional depth to bedrock and bedrock lithology information. A test pit was also excavated in May 1998 in the area immediately north of PW98–03 and PW98–04 to provide lithologic information. The pit measured approximately 5 ft wide by 12 ft long and 15 ft deep.

Temporary piezometers were installed at each probe location for water level measurement and ground-water sample collection. Piezometers were constructed of 0.5-in diameter by 5-ft PVC screen (#10 slot) and casing sections, with threaded bottom plugs and slip-joint caps. The assemblies were installed either through the probe rods or open hole. The base of the screens were set at or within 1-ft of the bedrock surface, if possible. Annular space was backfilled with #10 - 20 silica sand to within 6-in of the ground surface. The remaining space was plugged with 0.25-inch bentonite chips that were hydrated with potable water.

All piezometers were surveyed for location and elevation (ground surface and top of casing) based on the Monticello Project Coordinate System. Borehole information and piezometer placement information is summarized in Tables 3–1 and 3–2, respectively. Piezometers PW98–01 through PW98–07 were abandoned on July 27, 1998. Casing and screen were manually pulled and the boreholes were backfilled with granular bentonite to ground surface. Abandonment of the remaining piezometers is pending. Borehole and piezometer completion logs are included in the appendices.

In 1992, eight borings associated with the OU III remedial investigation were completed in the area of interest using a truck-mounted drill rig and hollow-stem augers (see Figure 3–1). Augering and continuous sampling was conducted until refusal in the bedrock. A 140-lb drop hammer with a 30-in drop was used to drive a 3-in o.d. by 24-in long split spoon sampler ahead of the auger bit to collect samples. The sampler was driven 24-in or until sampler refusal (≥50 blows for 6-in penetration). Observation wells were installed at several locations. Borehole and well completion logs from the 1992 investigation are also included in the appendices.

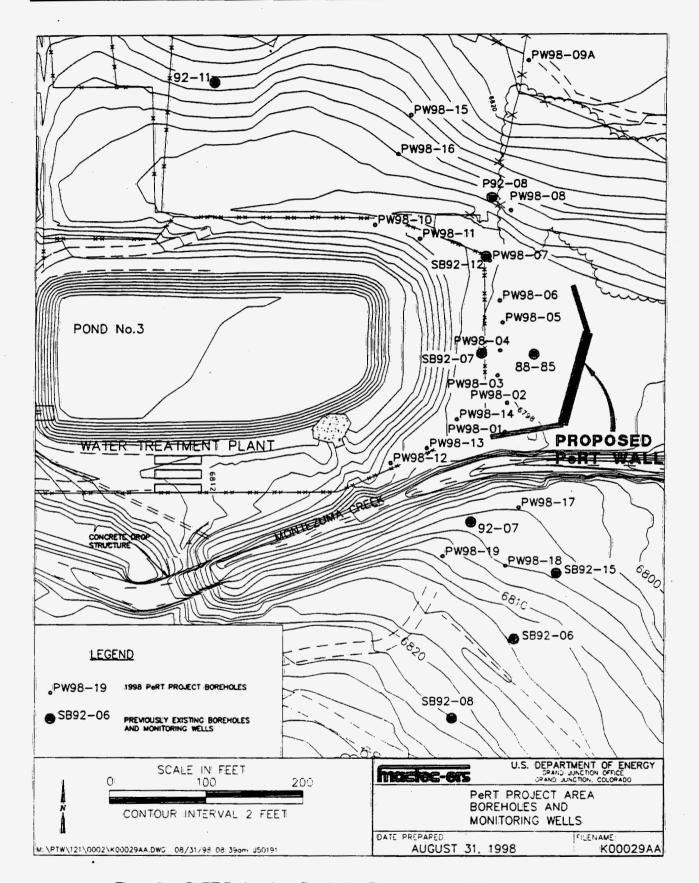


Figure 3-1. PeRT Project Area Boreholes, Piezometers, and Monitoring Wells

Table 3–1 Borehole Summary Data

Borehole	Date Completed	Northing	Easting	Ground Elev. [ft]	Hole Depth [ft]
PW98-01	5/28/98	10254.22	23954.26	6798.3	15.5
PW98-02	5/28/98	10287.32	23954.23	6798.1	15.5
PW98-03	5/28/98	10315.28	23946.81	6797.2	16
PW98-04	5/29/98	10339.84	23947.84	6797.4	16
PW98-05	5/29/98	10368.75	23948.01	6797.3	13
PW98-06	5/29/98	10391.19	23945.01	6797.7	14
PW98-07	6/01/98	10431.53	23935.08	6798.6	16
PW98-08	6/02/98	10485.35	23956.43	6805.3	18
PW98-09A	6/02/98	10638.78	23974.43	6822.7	12.5
PW98-10	6/02/98	10469.83	23816.40	6802.3	16
PW98-11	6/02/98	10453.82	23864.19	6801.3	17
PW98-12	6/03/98	10223.02	23837.14	6803.1	20
PW98-13	6/03/98	10239.13	23874.66	6800.5	17
PW98-14	6/03/98	10269.20	23904.94	6799.1	15.5
PW98-15	6/04/98	10582.83	23855.55	6810.3	14
PW98-16	6/04/98	10541.67	23841.38	6805.7	20
PW98-17	6/08/98	10178.12	23965.47	6801.3	19.5
PW98-18	6/08/98	10118.72	23953.77	6804.0	23.5
PW98-19	6/09/98	10125.03	23889.96	6807.5	25

Table 3-2 Piezometer Summary Data

Piezometer	Elev. Top of Casing [ft]	Stickup [ft]	Top of Screen bgs [ft]	Base of Screen bgs [ft]	Depth to Bedrock bgs [ft]
PW98-01	6799.44	1.14	8.9	13.9	14.3
PW98-02	6798.64	0.54	8.2	13.2	13.8
PW98-03	6797.56	0.36	9.6	14.6	14.1
PW98-04	6798.19	0.79	6.7	11.7	12.5
PW98-05	6798.10	0.80	5.8	10.8	11.5
PW98-06	6798.30	0.60	8.1	13.1	12.3
PW98-07	6800.17	1.57	8.4	13.4	14.3
PW98-08	6805.85	0.55	11.7	16.7	16.5
PW98-09A	6823.19	0.49	6.6	11.6	12
PW98-10	6803.99	1.69	8.3	13.3	13.8
PW98-11	6802.43	1.13	9.4	14.4	16.4
PW98-12	6804.14	1.04	14	15	18.4
PW98-13	6801.36	0.86	10.2	15.2	16.3
PW98-14	6800.61	1.51	8.5	13.5	14.5
PW98-15	6810.87	0.57	5.8	10.8	10.8
PW98-16	6806.81	1.11	10.3	15.3	16.8
PW98-17	6801.42	0.12	13.4	18.4	18.5
PW98-18	6803.94	-0.06	15.5	20.5	21.1
PW98-19	6807.51	0.01	19.5	24.5	24.8

bgs = below ground surface.

#### 4.0 Results

#### 4.1 Lithology of Unconsolidated Materials

The unconsolidated deposits in the PeRT project area consist of a layer of fine sandy silt that overlies saturated granular alluvium (sand, gravel, and cobbles). The Geoprobe® rig experienced little difficulty penetrating the upper layer of fine grained material, which was typically 6 to 10 ft thick in the valley floor north of the creek. The penetration rate through the fine materials (without sampling) was on the order of  $\geq 1$  foot per minute (ft/min).

Probe penetration of the underlying granular materials was successful at each location but required additional time and effort. Probing was hampered mainly when cobbles were encountered, often requiring 5 or 10 minutes of driving to displace or break an individual cobble.

In the absence of cobbles, the penetration rate of the probe (without sampling) was about 0.5-ft/min. Cobbles were encountered at most or all locations. Observations of test pit spoils indicated that the alluvial materials were primarily mixtures of sand and fine to coarse gravel (0.19 - 2.9 in, Unified Soil Classification System [USCS]) with some cobbles (2.9 - 11.8 in, USCS). The largest materials exhumed were two boulders that measured approximately 2 to 2.5 ft in length by 1.5 ft in diameter.

Along the base of the slope at and north of PW98–08 and PW98–15 (Figure 3–1), the upper layer of fine grained materials and basal sand and gravel layer terminates against colluvial deposits that consist of a mantle of cobbles with interstitial silt and sand that overlies sandy silt with clay and some gravel. Thin layers of peat and silty clay containing abundant organic carbon were encountered near the bedrock surface at locations PW98–08 and PW98–15. At PW98–09A, located on the terrace above the slope break, the cobble layer extended 12 ft to bedrock. The cobble layer was approximately 5 ft thick at PW98–15. As indicated in Figure 3–1, the PeRT wall is not expected to extend into this area of cobbles. A summary of the subsurface lithology and blow count information obtained during the 1992 investigation is presented as Table 4–1.

## 4.2 Bedrock Lithology

The upper bedrock at all but 3 locations (see below) probed during 1998 consisted of mudstone or siltstone within the middle portion of the Dakota Sandstone Formation. The probe penetrated up to 2 ft of bedrock at some locations. The upper 0.5 to 1 ft interval typically consisted of soft, cohesive, moist to wet clay that was easily penetrated. This upper interval was often weathered to a yellowish gray color. At some locations the upper bedrock was a medium stiff clay that was only slightly moist and more difficult to penetrate. With depth, the material generally graded to a dark gray, medium stiff to stiff clay with lower moisture content and greater resistance to penetration. The total thickness of the upper mudstone beds and the lithology of the underlying beds cannot be determined from the available data.

Table 4-1 Summary of 1992 Borehole Data

Borehole	Thickness of Fine Grained Layer [ft]	Thickness of Granular Layer [ft]	Blow Counts/6-in, Fine Grained Layer	Blow Counts/6-in, Granular Layer
88-85	7	5.5	15 to 21	>50
92-07	14	6.3	5 to 13	18 to 40
92–11	8	6	2 to 16	18 to 38
P92-08	4.5	6.5	6 to 38	16 to 55
SB92-06	26	4	4 to 18	20 to 32
SB92-07	6	7	3 to 15	22 to >50
SB92-08	27	3.5	7 to 15	33 to >50
SB92-12	6	7.5	2 to 12	18 to 29
SB92-15	17	4	3 to 10	18 to 46

Interbedded coal stringers were present within the 1.5 ft interval of dry mudstone recovered at PW98–15. At PW98–09A, 0.5 ft of dry coal/carbonaceous mudstone was recovered. Bedrock recovery at location PW98–03 consisted of 0.1 ft of dry carbonaceous mudstone or coal. The upper bedrock at each of the 1992 borehole locations also consisted of gray mudstone and siltstone, except at SB92–08, where dense sandstone was encountered. The sandstone layer occurs at a higher elevation than the mudstones encountered in the central portion of the valley floor (see Figure 4.5–2). Augering was generally discontinued about 0.5 ft into the bedrock but up to 1.5 ft were penetrated at locations 92–07 and P92–08.

#### 4.3 Depth to Ground Water

Depth to ground-water measurements taken in piezometers and existing monitoring wells in the project area during June and July 1998 are summarized Table 4.3–1. During that period, the elevation of the water table decreased from its highest position on June 9 to its lowest on July 22. The depth to water increased between about 0.5 to 0.7 ft at most locations. However, at locations PW98–08 and PW98–16, which are along the northern margin of the area investigated, water levels decreased by approximately 1 to 1.8 ft. Between July 22 and July 27, 1998, water levels increased on the order of 0.1 ft. Ground water was not present at locations PW98–09A and PW98–15 at any time.

Figure 4.3–1 illustrates the depth to ground-water below ground surface on June 19, 1998. Ground water was shallowest across the central portion of the valley floor between PW98–03 and PW98–07, ranging between approximately 4.5 and 5.5 ft below ground surface (June 19, 1998). At the remaining locations north of the creek, the depth to ground water varied between approximately 8.5 and 15 ft. Depth to ground water generally decreased with distance away from Pond 3. South of Montezuma Creek, the depth to ground water ranged from 16 to 22 ft.

Table 4.3-1 Ground-Water Level Summary Data

Piezometer/Well		6/09/98	i		6/19/98			6/24/98	=		7/16/98			7/22/98			7/27/98	
· 	DTW btoc [ft]	DTW bgs [ft]	Elev WT [ft]	DTW btoc [ft]	DTW bgs [ft]	Elev WT [ft]	DTW btoc [ft]	DTW bgs [ft]	Elev WT [ft]	DTW btoc [ft]	DTW bgs [ft]	Elev WT [ft]	DTW btoc [ft]	DTW bgs [ft]	Elev WT [ft]	DTW btoc [ft]	DTW bgs [ft]	Elev WT [ft]
PW98-01	9.95	8.8	6789.49	10.08	8.9	6789.36	10.15	9.0	6789.29	10.53	9.4	6788.91	10.54	9.4	6788.90	10.49	9.4	6788.95
PW98-02	7.51	7.0	6791.13	7.59	7.1	6791.05	7.68	7.1	6790.96	8.14	7.6	6790.50	8.15	7.6	6790.49	8.10	7.6	6790.54
PW98-03	4.99	4.6	6792.57	5.20	4.8	6792.36	5.37	5.0	6792.19	5.92	5.6	6791.64	5.93	5.6	6791.63	5.88	5.5	6791.68
PW98-04	5.59	4.8	6792.60	5.79	5.0	6792.40	5.97	5.2	6792.22	6.51	5.7	6791.68	6.55	5.8	6791.64	6.48	5.7	6791.71
PW98-05	5.18	. 4.4	6792.92	5.39	4.6	6792.71	5.59	4.8	6792.51	6.16	5.4	6791.94	6.19	5.4	6791,91	6.12	5.3	6791.98
PW98-06	5.30	4.7	6793.00	5.53	4.9	6792.77	5.73	5.1	6792.57	6.31	5.7	6791.99	6.33	5.7	6791.97	6.29	5.7	6792.01
PW98-07	7.08	5.5	6793.09	7.25	5.7	6792.92	7.46	5.9	6792.71	8.07	6.5	6792.10	8.09	6.5	6792.08	8.04	6.5	6792.13
PW98-08	11.99	11.4	6793.86	12.28	11.7	6793.57	13.08	12.5	6792.77	13.78	13.2	6792.07	13.82	13.3	6792.03	13.78	13.2	6792.07
PW98-09A	dry	dry	dry															
PW98-10	9.87	8.2	6794.12	10.11	8.4	6793.88	10.33	8.6	6793.66	11.03	9.3	6792.96	11.10	9.4	6792.89	10.99	9.3	6793.00
PW98-11	8.74	7.6	6793.69	8.94	7.8	6793.49	9.15	8.0	6793.28	9.83	8.7	6792.60	9.88	8.8	6792.55	9.79	8.7	6792.64
PW98-12	14.77	13.7	6789.37	14.87	13.8	6789.27	14.99	14.0	6789.15	15.24	14.2	6788.90	15.25	14.2	6788.89	15.18	14.1	6788.96
PW98-13	11.41	10.6	6789.95	11.52	10.7	6789.84	11.61	10.8	6789.75	11.94	1:1.1	6789.42	11.97	11.1	6789.39	11.91	11.1	6789.45
PW98-14	9.38	7.9	6791.23	9.52	8.0	6791.09	9.64	8.1	6790.97	10.07	8.6	6790.54	10.10	8.6	6790.51	10.05	8.5	6790.56
PW98-15	dry	dry	dry	dry	dry	dity												
PW98-16	12.24	11.1	6794.57	12.50	11.4	6794.31	12.75	11.6	6794.06	13.46	12.4	6793.35	13.49	12.4	6793.32	13.41	12.3	6793.40
PW98-17	16.27	16.2	6785.15	16.42	16.3	6785.00	16.56	16.4	6784.86	16.79	16.7	6784.63	16.80	16.7	6784.62	16.72	16.6	6784.70
PW98-18	18.75	18.8	6785.19	18.98	19.0	6784.96	19.02	19.1	6784.92	19.49	19.6	6784.45	19.47	19.5	6784.47	19.26	19.3	6784.68
PW98-19	21.55	21.5	6785.96	20.14	20.1	6787.37	21.32	21.3	6786.19	21.36	21.4	6786.15	21.50	21.5	6786.01	21.13	21.1	6786.38
88-85	7.28	6.9	6790.23	7.41	7.0	6790.10	7.53	7.1	6789.98	7.69	7.3	6789.82	7.87	7.5	6789.64	7.42	7.0	6790.09
92-11	15.97	15.2	6797.76	កាកា 🏻	nm	nm	16:38	15.7	6797.35	nm	nm	nm	16.73	16.0	6797.00	nm	nm	nm
92-07	18.82	16.6	6787.03	18.62	16.4	6787.23	18.71	16.5	6787.14	ınm	nm	nm	19.03	16.8	6786.82	19.05	16.8	6786.80

DTW, btoc = depth to groundwater, below top of casing.

DTW, bgs = depth to groundwater, below ground surface.

Elev WT = elevation of water.

nm= not measured

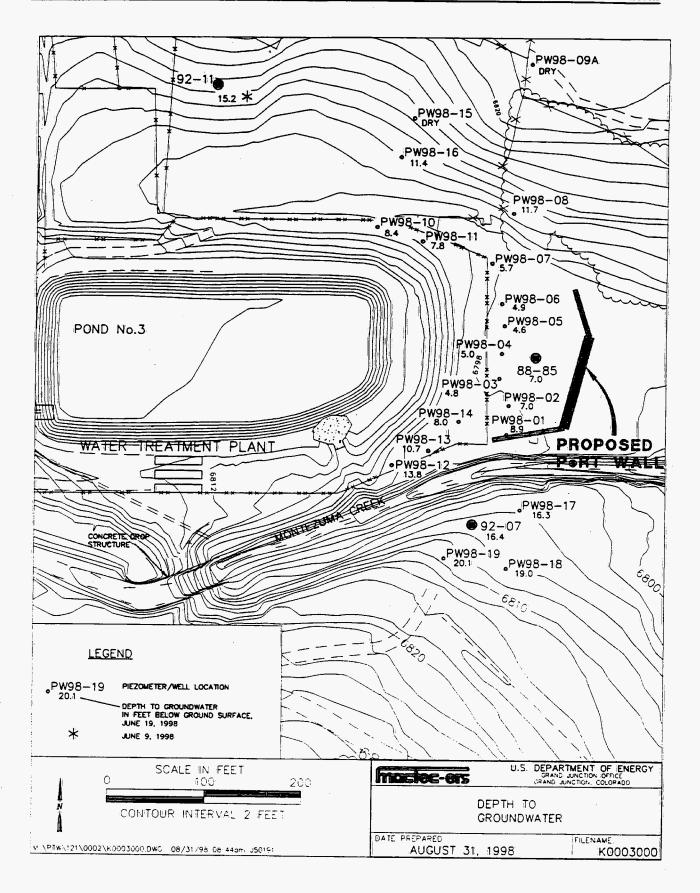


Figure 4.3-1. Depth to Ground Water Below Ground Surface, June 19, 1998

Since November 1992, the depth to ground water at well 88–85 has fluctuated between ±1 ft from an approximate mean of 7.5 ft below ground surface, except during April through July 1993, when ground water rose to within 1.5 ft of the surface. Similar peak water levels also occurred at wells 92–11 and P92–08, but not at 92–07 (see hydrographs in appendices), however, the July 1993 measurement at well 92–07 is suspect. Although hydrographs for many other site monitoring wells exhibit relatively high water levels during mid-1993, leakage from a stock pond formerly in the Pond 3 area may have contributed to the high water levels of 1993 in wells 92–11, 88–85, and P92–08. Construction of Pond 3 was completed during the summer of 1994.

#### 4.4 Depth to Bedrock

Depth to bedrock and bedrock elevation results are presented in Table 4.4–1 and illustrated in map view in Figures 4.4–1 and 4.4–2, respectively. The depth to bedrock in the center of the project area (locations PW98–01 through PW98–07) ranges from 11.5 to about 14.5 ft below ground surface. The ground surface and bedrock surface in that area are relatively flat. Along the slope break between PW98–08 and PW98–16, the depth to bedrock increases slightly to approximately 16.5 to 17 ft. Immediately north of those locations, the bedrock surface rises significantly. In the vicinity of the proposed south funnel section of the PeRT system (locations PW98–01 and PW98–14), the depth to bedrock is approximately 14.5. The bedrock surface gradually slopes down to the southeast from the north side of Montezuma Creek in the area of investigation and then rises steeply approximately 250 ft south of the creek near location SB92–08. The bedrock surface is approximately 3 to 4 ft below the creek bed in the project area. At the eastern base of the drop structure however, Dakota Sandstone is believed to outcrop in the creek bed.

The available data indicate that the saturated thickness of the aquifer south of the creek (approximately 2.5 to 4 ft) is generally several feet less than on the north side (approximately 5.5 to 9.5 ft). This may be due to the close proximity of the piezometers to mounded ground water around Pond 3, or a broadening of the bedrock valley south of the creek. The saturated thickness of the alluvial aquifer is shown in map view in Figure 4.4–3 for June 19, 1998, and in tabular form in Table 4.4–2 for each measurement event. Locally, the northern limit of the aquifer is interpreted to coincide with the slope break in ground surface and bedrock topography that extends from PW98–15 to immediately north of PW98–08, and then for an undetermined distance east along the base of the cobbled terrace deposit (see Figure 4.4–3).

#### 4.5 Ground-Water Flow

Figure 4.5–1 illustrates the surface of the alluvial aquifer based on the June 19, 1998 measurement data. Comparing Figure 4.5–1 and 4.4–2 indicates that the water table surface and corresponding direction of ground-water flow (perpendicular to ground-water elevation contour lines) is strongly influenced by the topography of the bedrock surface. The prominent feature of the water table map is the change in the direction of flow from predominantly southeast in the area northwest of the PeRT wall to south-southeast in the vicinity of 98–03 and 98–14. Ground water then flows beneath Montezuma Creek from the north in a south-southeasterly direction. The creek intersects the water table but is not an aquifer discharge or recharge boundary, although some seepage to and from the stream banks is likely. On the south side of the creek, the direction of flow again becomes southeast to east-southeast.

Table 4.4-1 Bedrock Surface Summary Data

Borehole	Ground Elev. [ft]	Depth to Bedrock, bgs [ft]	Bedrock Elev. [ft]
PW98-01	6798.3	14.3	6784.0
PW98-02	6798.1	13.8	6784.3
PW98-03	6797.2	14.1	6783.1
PW98-04	6797.4	12.5	6784.9
PW98-05	6797.3	11.5	6785.8
PW98-06	6797.7	12.3	6785.5
PW98-07	6798.6	14.3	6784.4
PW98-08	6805.3	16.5	6788.8
PW98-09A	6822.7	12	6810.7
PW98-10	6802.3	13.8	6788.5
PW98-11	6801.3	16.4	6784.9
PW98-12	6803.1	18.4	6784.7
PW98-13	6800.5	16.3	6784.2
PW98-14	6799.1	14.5	6784.6
PW98-15	6810.3	10.8	6799.5
PW98-16	6805.7	16.8	6788.9
PW98-17	6801.3	18.5	6782.8
PW98-18	6804.0	21.1	6782.9
PW98-19	6807.5	24.8	6782.7

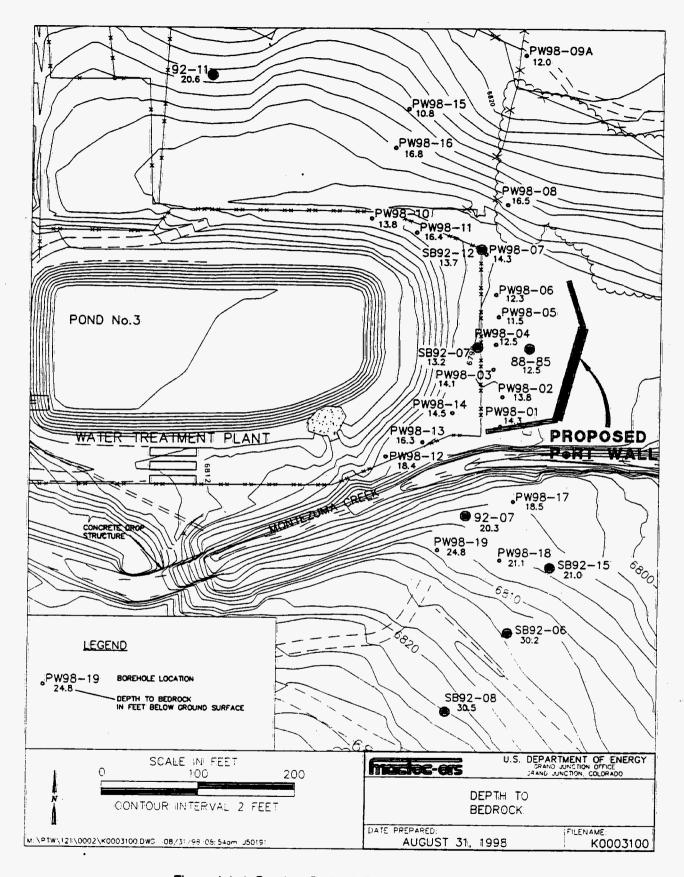


Figure 4.4-1. Depth to Bedrock Below Ground Surface

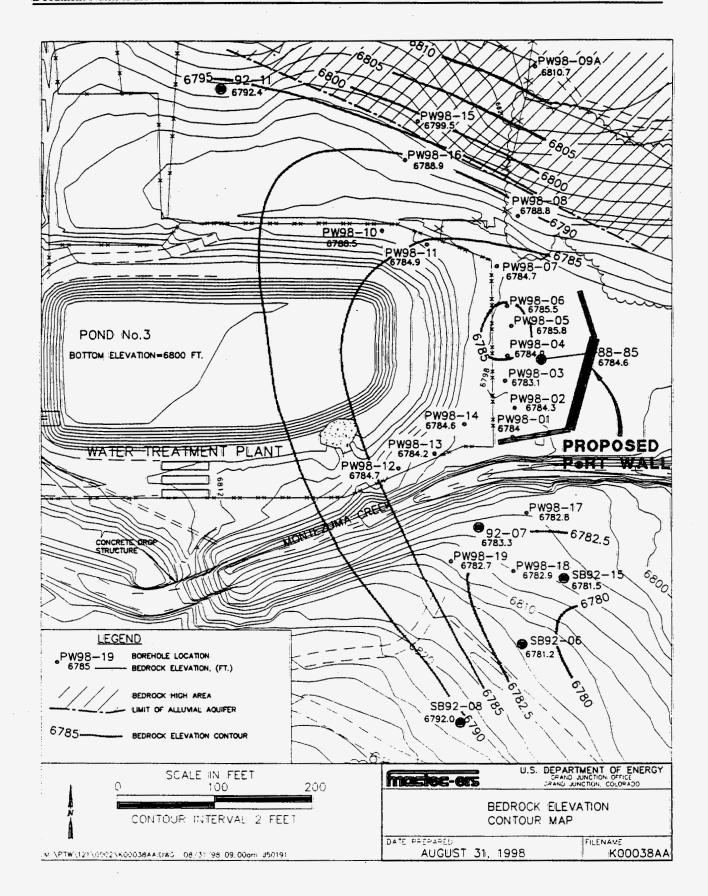


Figure 4.4-2. Bedrock Elevation Contour Map

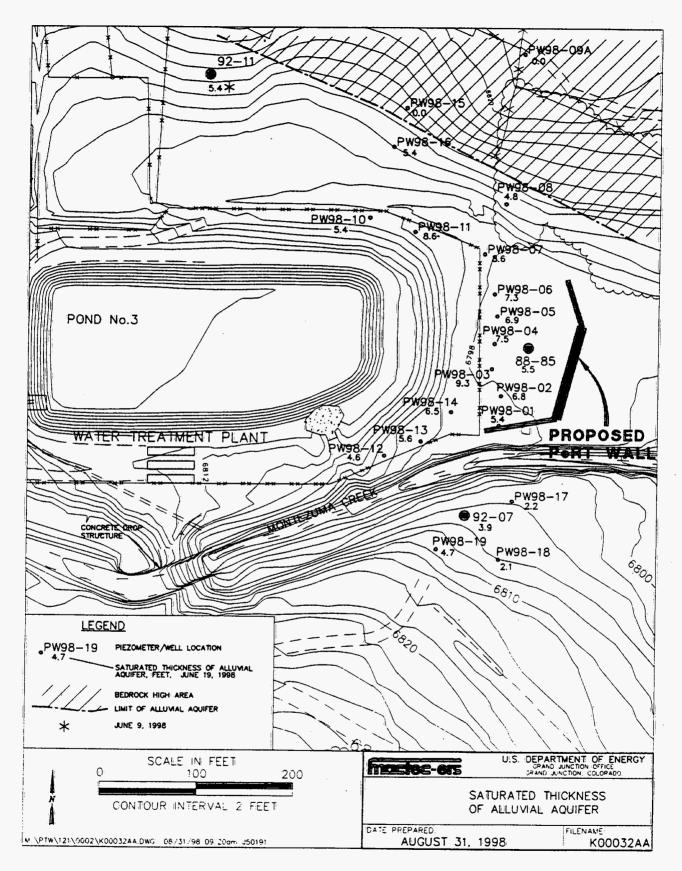


Figure 4.4-3. Saturated Thickness of Alluvial Aquifer, June 19, 1998

Table 4.4-2 Saturated Thickness of Alluvial Aquifer

			Saturated T	hickness [ft]			
Borehole	6/9/98	6/19/98	6/24/98	7/16/98	7/22/98	7/29/98	
PW98-01	5.5	5.4	5.3	4.9	4.9	4.9	
PW98-02	6.8	6.8	6.7	6.2	6.2	6.2	
PW98-03	9.5	9.3	9.1	8.5	8.5	8.6	
PW98-04	7.7	7.5	7.3	6.8	6.7	6.8	
PW98-05	7.1	6.9	6.7	6.1	6.1	6.2	
PW98-06	7.5	7.3	7.1	6.5	6.5	6.6	
PW98-07	8.7	8.6	8.4	7.8	7.7	7.8	
PW98-08	5.1	4.8	4.0	3.3	3.2	3.3	
PW98-09A	0	0	0	0	0	0	
PW98-10	5.6	5.4	5.2	4.5	4.4	4.5	
PW98-11	8.8	8.6	8.4	7.7	7.7	7.7	
PW98-12	4.7	4.6	4.4	4.2	4.2	4.3	
PW98-13	- 5.7	5.6	5.5	5.2	5.2	5.2	
PW98-14	6.6	6.5	6.4	5.9	5.9	6.0	
PW98-15	0	0	0	0	0	0	
PW98-16	5.7	5.4	5.2	4.4	4.4	4.5	
PW98-17	2.4	2.2	2.1	1.8	1.8	1.9	
PW98-18	2.3	2.1	2.0	1.5	1.6	1.8	
PW98-19	3.3	4.7	3.5	3.4	3.3	3.4	
88–85	5.6	5.5	5.4	5.2	5.0	5.5	
92–11	5.4	ND	5.0	ND	4.6	ND	
92–07	3.7	3.9	3.8	ND	3.5	3.5	

ND = no data

Figure 4.5–1 also indicates that the hydraulic gradient steepens from northwest to southeast. The steepening is not caused by a change in the slope of the bedrock because of the relatively flat bedrock surface in the area. The steepened hydraulic gradient may instead result from a narrowing of the aquifer in the area of the bedrock high, and/or the presence of less transmissive sediments along the north margin of the aquifer, and/or local ground-water mounding around Pond 3.

Figure 4.5–2 presents a north-south sectional view of the integrated subsurface information described in the preceding sections. The elevation of the creek stage and bed, as shown in Figure 4.5–2, were obtained during a previous investigation.

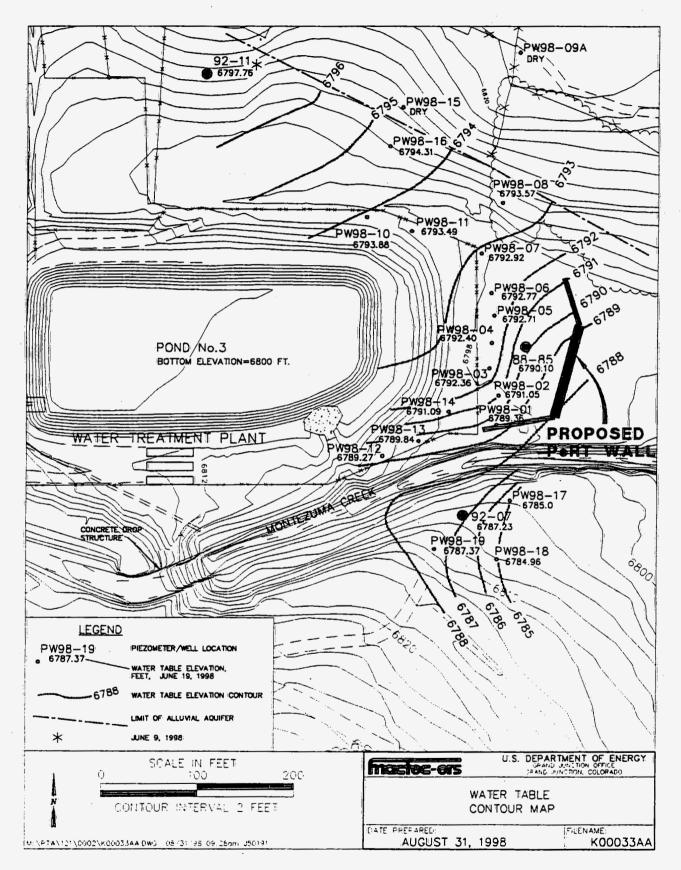


Figure 4.5-1. Alluvial Aquifer Water Table Contour Map, June 19, 1998

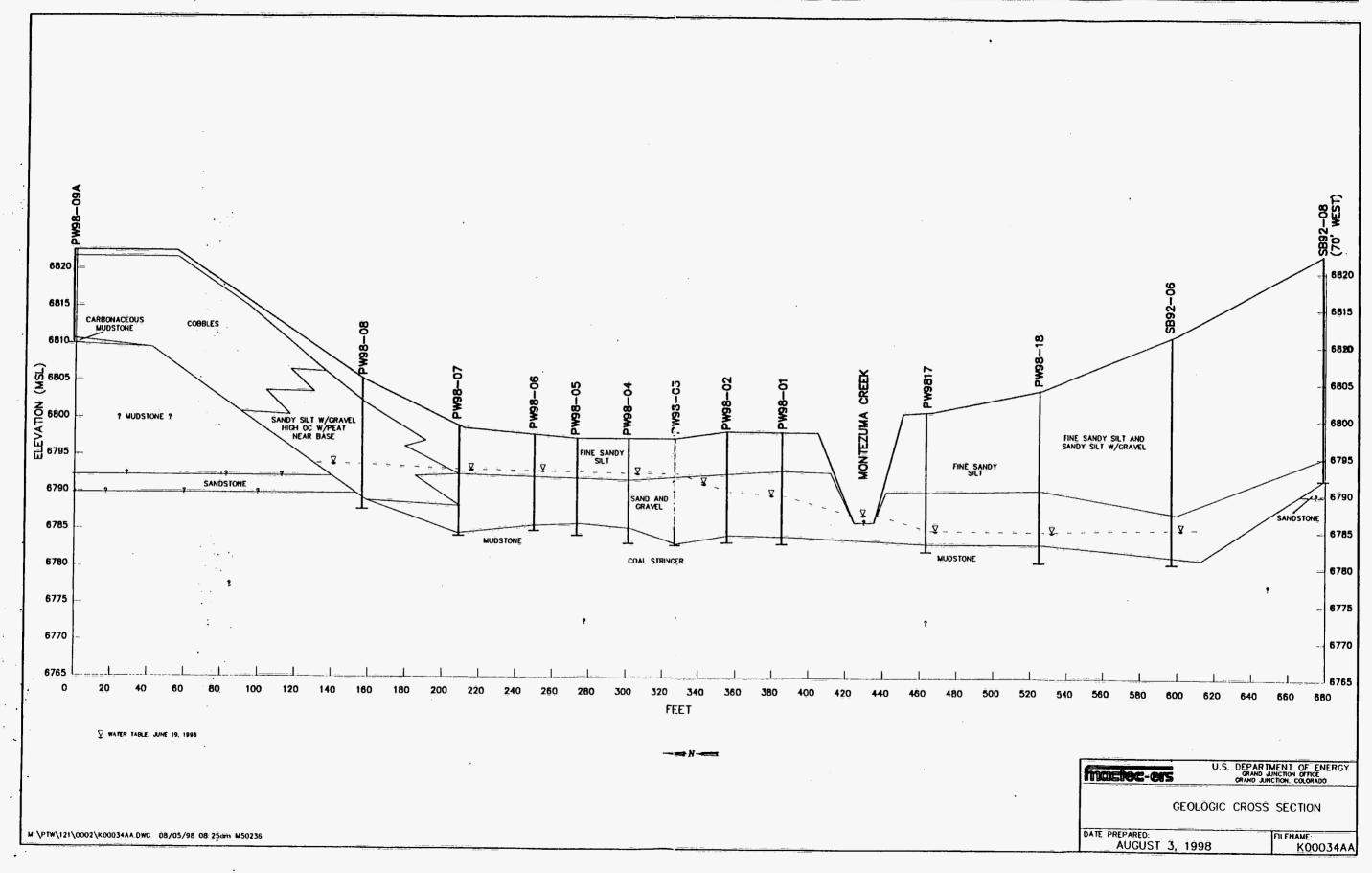


Figure 4.5-2. Geologic Cross Section

#### 4.6 Ground-Water Sampling

A ground-water sample was collected for laboratory analysis from each piezometer on June 9, 1998. Prior to sample collection, piezometers were surged and pumped cyclically to remove fine grained sediments that had accumulated inside the screen during installation. Sample collection was also preceded by purging the piezometer for about 15 to 20 minutes at flow rates of 0.5 to 1 liter/min. Field parameters (e.g., pH, temperature, conductivity) were not measured during the purge, however previous sampling conducted at the site indicates that the purge was sufficient to achieve parameter stability. In most cases, a relatively clear, low-turbidity sample was collected. Samples were withdrawn using HDPE tubing and peristaltic pump and collected in 250-mL HDPE containers. All samples were kept in ice baths or refrigerated until analysis.

The ground-water samples were analyzed for uranium at the Grand Junction Office Environmental Sciences Laboratory on June 11, 1998. Prior to analysis, samples were filtered through 0.45 µm membrane filters. Samples were then analyzed by laser induced fluorescence using a Scintrex UA-3 uranium analyzer.

Results of the analyses are summarized in Table 4.6–1 and illustrated in map view in Figure 4.6–1. The map distribution shows that the lowest concentrations were detected in samples collected at PW98–16 and PW98–08 (0.38 and 0.19 mg/L, respectively), which are located along the northern margin of the aquifer. A consistent trend of increasing uranium concentrations is then observed from north to south between locations PW98–08 and PW98–01 on the north side of the creek, and continues south of the creek to locations PW98–17 and 92–07. Farther south, uranium concentrations increase significantly at locations PW98–18 and PW98–19, where the maximum values were detected (3.6 and 4.2 mg/L, respectively). The maximum concentrations (locations PW98–18 and PW98–19) are comparable with those detected in samples collected previously from well 82–36A (2.6 to 4.1 mg/L), which is located 700 ft to the northwest in the southeast portion of the East Tailings Pile near the millsite boundary. In samples collected previously from well 92–11, uranium concentrations ranged between 1.4 and 2.9 mg/L. These results are comparable with concentrations detected at PW98–10, PW98–12, PW98–13, and PW98–14.

The distribution of uranium is interpreted to represent a composite plume consisting of 2 lobes (Figure 4.6–1). The southern extension, which has higher concentrations, may originate directly from the southeast area of the East Tailings Pile, where mill tailings are believed to extend well below the water table. Uranium is subsequently transported from that area in a relatively narrow plume that is oriented northwest to southeast and extends between the drop structure and a line connecting locations 92–07 and PW98–12. Because the creek is not a hydraulic barrier in this area, the lobe extends south of the creek, and is positioned west and south of the proposed PeRT wall. Concentrations of uranium in Montezuma Creek are much too low to account for the increased levels in ground water south of the creek.

The northern lobe generally occupies the area between wells 92–07 and 92–11, and may represent the combined input from other, more distant, source areas elsewhere on the millsite. The axis (most contaminated portion) of the northern lobe also extends in a southeasterly direction to the south and west of the proposed wall location.

Table 4.6-1 Ground-Water Sample Results

Sample Location	Uranium [mg/L]
PW98-01	1.01
PW98-02	0.979
PW98-03	0.841
PW98-04	0.625
PW98-05	0.704
PW98-06	0.574
PW98-07	0.465
PW98-08	0.192
PW98-10	1.09
PW98-11	0.818
PW98-12	1.46
PW98-13	1.70
PW98-14	1.54
PW98-16	0.379
PW98-17	1.25
PW98-18	3.61
PW98-19	4.18

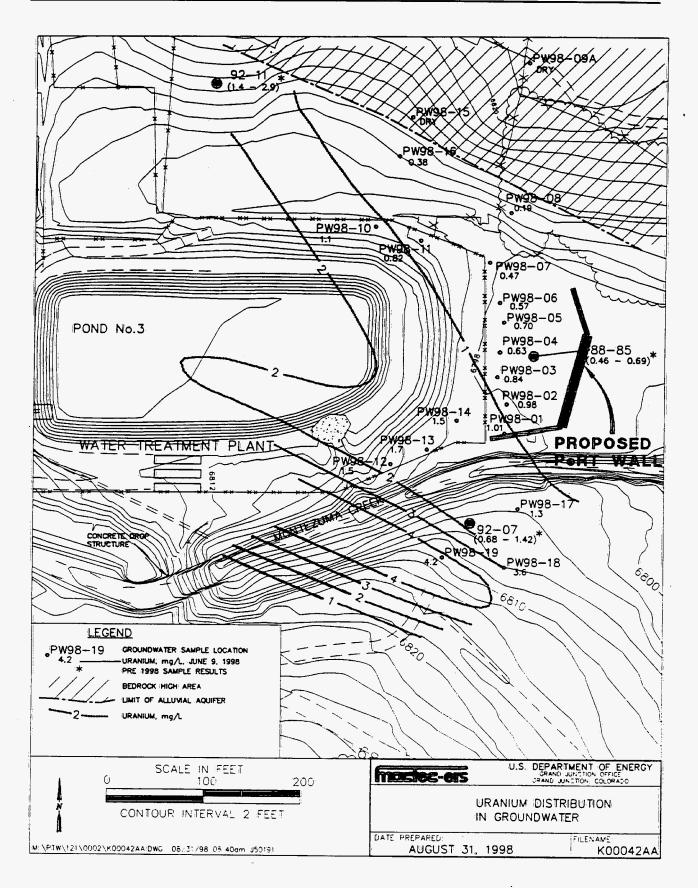


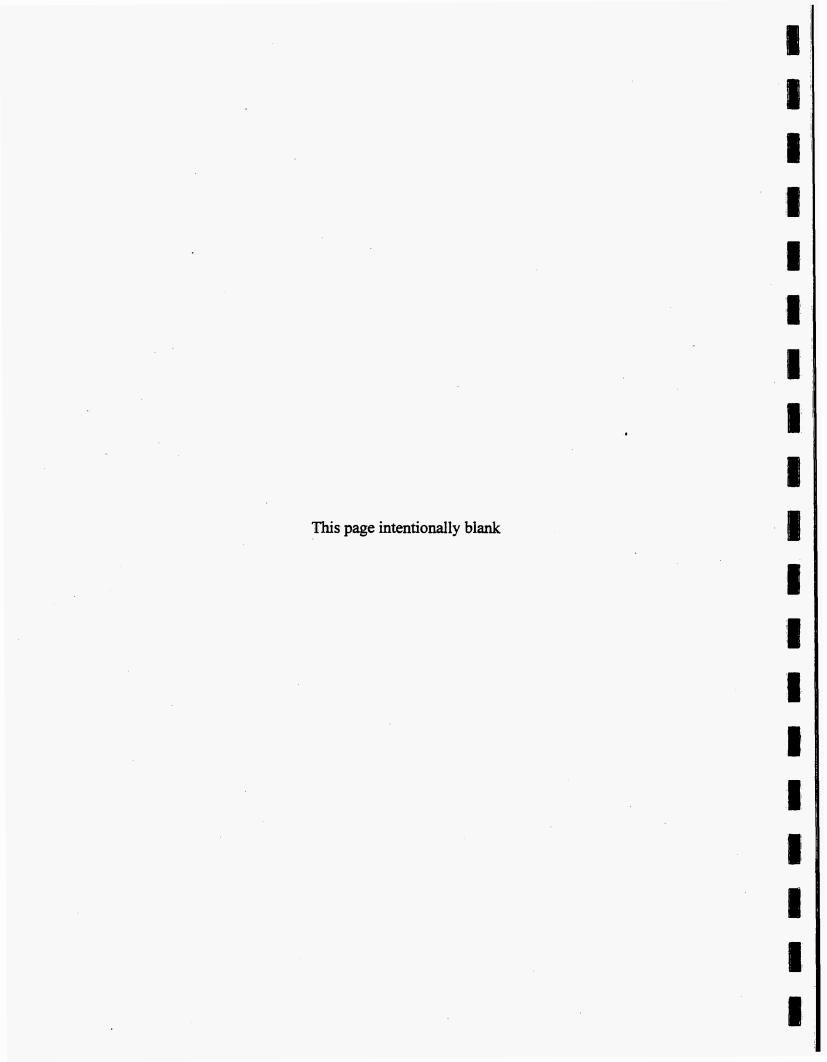
Figure 4.6-1. Uranium Distribution in Ground Water, June 9, 1998

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## 5.0 Recommendations for Further Characterization

The information presented above provides adequate characterization of the hydrogeology and uranium distribution in ground water north of Montezuma Creek in the PeRT project area. The information indicates that much of the uranium plume may extend farther south than previously anticipated. However, the boundaries of the alluvial aquifer and uranium plume, and groundwater flow in the area south of the creek cannot be determined from the available data. Because such information would benefit the PeRT project, the following tasks are suggested:

- Use the Geoprobe® rig to investigate 5 locations on the south side of Montezuma Creek (south of locations PW98–18 and PW98–19). Proceed south until the limit of the aquifer is encountered. Collect soil and bedrock samples and install temporary piezometer at each location.
- Use the Geoprobe® rig to investigate 3 locations in the vicinity of the water treatment plant on the north side of Montezuma Creek (west of locations PW98–18 and PW98–19). Collect soil and bedrock samples and install temporary piezometer at each location.
- Use the Geoprobe® rig to investigate 2 locations on the south side of the creek near the top of the drop structure. Collect soil and bedrock samples and install temporary piezometer at each location.
- Survey new piezometer locations and elevations.
- Measure depth to ground water at new and existing well and piezometer locations.
- Collect ground-water samples at new and existing well and piezometer locations. Analyze samples for uranium.



# Appendix A

Borehole and Completion Logs, 1998 Field Program

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Borehole Summary

MACTEC-ERS

97 B 3/4 Road

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						Site	M	enticello Project PERT
30.	ell No		Pu	J 92	3-	02		Location (N) 10 287.32 (E) 23954. 23
					Bit/A	uger S		Zinch o.d. Hole Death (Ft) 15.5
ealant Frout ocking Filling l	Cover I	nstal	PYC PYC PYC PYC 10-70 9 bentonial N/A led Y (N) Feo p # 198 D Hett, h	rob ate D	Padlo evelo	ol. (cf.	(gal)	Interval (Ft.)  O to 8.2  Slot Size #10  Solot Size #10  Location Sketch  Sampling Method 2' Core barrel  Fluid Level/Date 7.59 5 50 6/19/98  Remarks Abandoned 7/27/98
(FT)	6°	ppm	Sample No Interval		WELL	JCTION	GRAPHIC LOG	C DESCRIPTION .
0	1							Required Information:  Typical name; Munsell color; percentage sand and gravel; sorting (poor to well); grain angularity; induration or plasticity; moisture content (moist to saturated).
	-2	-	12 - 13.5		2			Fush w/o sampling to 12'.  Sound w/ gravel + colibles, saturated
	-6 419/98-	$\nabla$	13.5-	Pack	Casi	ack		Recovered ~ 1'.  13.5'-13.8' Soul + gravel, saturated  13.8-14.5' mudstone, dense, sl.
	-10		_	Sand	Screen	Sand 1	-	mors &, gray.
	14		<b>7⊅</b> –				ravel destone	
			ground level.	#	-			

Borehole Summary

**MACTEC-ERS** 

**SACTEC-ERS** 

Facility N/A  Site Montricello  Project PERS  Boring/Well No. PW98-04  Cocation (N) 10339.84 (E) 23947.  Ground Elev. (Ft.) 6797.4 Bit/Auger Size Z inch o.d.  Diameter (inch I. D.)  TYPE Vol. (cf. gal) Interval (Ft.)  Screen  PVC 0.5 in 0 to 6.7  Slank Casing PVC 0.5 in 0.7 to 1.7  Summy/End Cap PVC 0.5 in 11.7 to 118  Scand Pack 10-70 5/1/ce 0.5 to 16  Grad Pack 10-70 5/1/ce 0.5 to 16  Grad Cover Installed Y RD Padlock No. N/A  Orilling Method 12 core barrel  Date Drilled 1729/98 Date Developed N/A  Fluid Level/Nate 15.	2597	TEC-E B 3/4	Roa		. 04	<b>500</b>			Borehole Summa
Boring/Well No. PW 18 - 04  Ground Elev. (Ft.) 6797. # Bit/Auger Size Zinch o.d.   Location (N)   10339.8 # (E)   23147.    Diameter (inch i. D.)   No. of Completions   Location (N)   Location (N								. 4.	
Bit/Auger Size Zinch o.d.  Diameter (inch 1. D.)  Vol. (cf. gail)  TYPE  Vol. (cf. gail)  Fig. 2.5 in				Dila	0		Site	- ///	ontilello Project FEAT
Diameter (Inch I. D.)  Vol. (cf. gal)  Vol. (c						- 0	24		Location (N) /0339.84 (E) Z3947.84
Stick-Up Height (Ft)  Stick-Up Height (Ft)  Creen  PVC	Ground	Elev. (F	t.) _	6797.4	<u>-</u>				Z inch o.d. Hole Depth (Ft)
Construction   Cons		asing	•	PVC		V.	ol. (c)	. gal)	Interval (Ft.) Stick-Up Height (Ft) 0.79
and Pack ealant from the first of the standards depth ocking Cover Installed Y (1) Padiock No. N/A  ocking Cover Installed Y (2) Padiock No. N/A  sampling Method Copyrole  Sampling Method Z' core burned  Fluid Level/Date 5' 635 0/9/92.  Remarks Abandoned 7/22/92 of 1/9/92.  Remarks Abandoned 7/22/92 of 1/9/92.  Required Information:  Typical name; Munsell color; percentage sand and gravel; sorting (p to well); grain angularity; induration or plasticity; moisture content (m to saturated).  Pished W Sampling to 12'.  A 1/11/18 V (1) Page 1/1		nd Cao	•						4.7 to 11.7 Location Sketch
realiant from the chips ocking Cover Installed Y (10) Padlock No. N/A  sampling Method Septole  Sampling Method Septole  Sampling Method Septole  Fluid Level/Date 5 ' 6.5. 6/19/19.  Remarks Abandoned 7/27/19.  Dapth 8   PID Sample No.; WELL CONSTRUCTION CLOG    Proper Interval   Construction Constructio	Sand Pa		•		Sili				
Ocking Cover Installed Y (1), Padlock No. N/A  Filling Method George  Sampling Method Top From  Filling Method George  Sampling Method Top From  Filling Level/Date Single  Filling Lev			-	benton	te	Chief	25		
Trailing Method  See Probe  Trailing Method  Trailing Met		Cover I	- nstal	led Y (N)	<del>_</del> ,	Padlo	ck No	N/A	4
ampler(s)    Depth   Blower   PID   Sample No.;   WELL   Interval   CONSTRUCTION   CONSTRUCTION	rilling I	Method		Geopro	Le				Sampling Method 2' core bassel
Depth' Blows   PID   Sample No.;   WELL   CONSTRUCTION   Log    Required Information: Typical name; Munsell color; percentage sand and gravel; sorting (p to well); grain angularity, induration or plasticity; moisture content (m to saturated).    Value			729	1/98 Da	te Do	evelo	ped _	NA	Fluid Level/Date 5 695 6/19/42
Required Information: Typical name; Munsell color; percentage sand and gravel; sorting (p to well); grain angularity; induration or plasticity; moisture content (m to saturated).  Pushed w/o sampling to 12'.  4 - 6/11/18 \rightarrow  12-14' \rightarrow  1 - 12-14' \rightarrow  Send + gravel.							EVIA	<del></del>	7 10 10 10 10 10 10 10 10 10 10 10 10 10
Typical name; Munsell color; percentage sand and gravel; sorting (p to well); grain angularity; induration or plasticity; moisture content (m to saturated).    Fished of Sampling to 12'.							JCTION	LOG	DESCRIPTION
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12-14   recovery: 12-12.5' souturated	17=	.			. "			Sandy	
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MACTEC-ERS

Borehole Summary

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**MACTEC-ERS** 

2597 B 3/4 Road

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		,	Colorado					•
-acility	N	14	<u>.</u>			Site	M.	lonticello PERT
3oring/	Well No	·	PW99	3 -	OK	2		Location (N) /0 391.19 (E) 23945.01
Ground	Elev. (F	t.) _	6797.7	<u> </u>				Zinch o.d. Hole Depth (Ft)
			TYPE			amete ol. (cf.	r (inch nall	No. of Completions
3lank C	_		PIC	_		.5		Interval (Ft.)  O to S./  Slot Size #10
Sump/E	nd Cap	-	PUL			<del>],                                    </del>	<del></del>	8./ to /3./ Location Sketch
Sand Pa	ack	•	10-20	25,1	ica	<u> </u>		13.1 to 13.2 2.5 to 14
Sealant Grout		-	Bentoni					0 to 0.5
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	l						:	Pushed to 10' w/o sampling
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				1		3		12.9 gity muistone w/ some line
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MACTEC-ERS 597 B 3/4 Road Grand Junction, Col			Borehole Sum Page	
cility N/A	· · · · · · · · · · · · · · · · · · ·	site Monticello	Project PERT	
Boring/Well No. P	N98-07	7	Location (N) 10431.53 (E) 23935.	. 08
4 <b></b> :	Dia	ager Size Zinch o.d.	Hole Depth (Ft)	
Streen Sump/End Cap Ind Pack	-zo silica	(cf. gal)   Interval (F   0 to 8.   8.4 to 13.   13.4 to 13.	Slot Size #10 Lecation Sketch	7
Grout	N/A - Chi	0 to 0.	<u> </u>	
Date Drilled 6/1/98 Sartlett	Pate Develop	ped N/A Sam	right pling Method 2 core burel  Fluid Level/Date 5.7 bys 6/19/92  S Abandoned 7/27/98	
	mple No.; WELL nterval CONSTRU	CTION LOG DESCRIPTION		
6/19/98 7	Sand lack Screen Lusing	to well); grain a to saturated).  Push to lo' was leavered 3" silty see 12-12.5"  12-12.5"  14-14.25	Munsell color; percentage sand and gravel; sorting (pangularity; induration or plasticity; moisture content (management)	noist

All depths measured from ground level.

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empleted By T. Bartlett

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MACTEC-ERS  Borehole Summai  2597 B 3/4 Road  Page _/_ of _/  Grand Junction, Colorado 81502
Facility N/A Site Monticello Project Pert
Boring/Well No. PW98-09A Location (N) 10638.78 (E) 23974.43
Ground Elev. (Ft.) 6872.7 Bit/Auger Size Zinch o.d. Hole Depth (Ft) 17.5  Diameter (inch I. D.) No. of Completions/
Blank Casing PVC QS in Q to C.6 Slot Size \$\frac{10}{2}\$ O to C.5 in Constant \$\frac{10}{2}\$ O to C.5 in Constant \$\frac{10}{2}\$ O to C.5 Slot Size \$\frac{10}{2}\$ O to C.5 Slot
Sampler(s) Bartlett, Worth, Trevino Remarks
Depth* Blows/ PID Sample No.: WELL GRAPHIC DESCRIPTION  (FT) 5" ppm Interval CONSTRUCTION LOG
Required Information: Typical name; Munsell color; percentage sand and gravel; sorting (poor to well); grain angularity; induration or plasticity; moisture content (moist to saturated).  Pushed who Sampling to 5'.  V. difficult push, recovered ignerus culbbles frequents, dry.  Typical name; Munsell color; percentage sand and gravel; sorting (poor to well); grain angularity; induration or plasticity; moisture content (moist to saturated).  Pushed who Sampling to 5'.  V. difficult push recovered ignerus culbbles frequents, dry.  Typical name; Munsell color; percentage sand and gravel; sorting (poor to well); grain angularity; induration or plasticity; moisture content (moist to saturated).  Pushed who Sampling to 5'.  V. difficult push recovered ignerus culbbles frequents, dry.  Typical name; Munsell color; percentage sand and gravel; sorting (poor to well); grain angularity; induration or plasticity; moisture content (moist to saturated).  Pushed who Sampling to 5'.  V. difficult push recovered ignerus culbbles frequents, dry.  Typical name; Munsell color; percentage sand and gravel; sorting (poor to well); grain angularity; induration or plasticity; moisture content (moist to saturated).  Pushed who Sampling to 5'.  V. difficult push recovered ignerus culbbles frequents, dry.  Typical name; Munsell color; percentage sand and gravel; sorting (poor to well); grain angularity; induration or plasticity; moisture content (moist to saturated).  Pushed who Sampling to 5'.  V. difficult push recovered ignerus culbbles frequents, dry.  Typical name of the first push recovered ignerus culbbles frequents, dry.  Typical name of the first push recovered ignerus culbbles frequents, dry.  Typical name of the first push recovered ignerus culbbles frequents.  Typical name of the first push recovered ignerus culbbles frequents.  Typical name of the first push recovered ignerus culbbles frequents.  Typical name of the first push recovered ignerus culbbles frequents.  Typical name of the first push recovered ignerus culbbles frequ
All depths measured from ground level.

Borehole Summar

Verified By

Borehole Summary

acility	4 .	Site	M	onticello		Project _	PERT
Boring/Well No.	PW98	-12		er i i	Location (N)	10223.02	(E) <u>Z3837.14</u>
Ground Elev. (Ft	1 6803.1	Diamet	er (inch I	Linch O.d.		Hole Depth (Ft)	70
lank Casing	TYPE PVC	Vol. (cf		Interval (Ft.)		Stick-Up Heigh Slot Size #/	
Screen	PVC	0.50	1	14 to 19		Location Sketch	
i <del>ump/</del> End Cap and Pack	10-20 S	0.50		19 to 19.1		1	
Sealant		e chips		0.5 to 20 0 to 0.5			
irout	NA		<del>=</del> ,				
ocking Cover In	Geoprobe	Padlock No	· _ <i>N/A</i>	Samol	ing Method 1	z' core be	errel
ate Drilled <u>6/3</u>	/98- Date	e Developed		Fit	uid Level/Date _	4.87 BTOC	
	Hett/Word	h/Yrevio	•	Remarks _			
Depth* Blows/ (FT) 6*	PID Sample No.; ppm Interval	CONSTRUCTION	GRAPHIC LOG	DESCRIPTION			
				Required Inform Typical name; M to well); grain and to saturated).	unsell color; perc	entage sand and n or plasticity; mo	gravel; sorting (poor isture content (moist
0 + -				Push to 6'	Sto Samuel	na V. eas	y push.
2+	8-10'			Sandy silt, 51	moist, v	i easy push	۲.
4	+ ,	-     -		9-10+ Sanda 9.5-10' San Sand + silt,	79V1. 9-	moist es	esy bush.
	10-12'		7		,	•	l.
6+			h.	13-14' Sand	w/ gv1. +		
8+	14-16	-	3	sand/qul./si		coldo les u	vet to
10-	16-18'	Lesis le	fine s	Cobble et 16 fines, satura	" then so	and + f c	c. gul., some
12	18-20	7 3	-		····	<del>.</del> /	
14- 4/19/98	∇   18-20	1 N	ave/ les s	Sand + grave 18.4' - 19.4 5.	ft, grade	rellow to gray	clay,
16-		- 12 -	e tre		of moist.		
18		560	5 pm 6 1 5 pm 4 5 pm				
70	TD		muds tone				
All depths measured ompleted By	from ground level. T. Bartlet	<del>t-</del>	Veri	fied By			

2597	TEC-EI B 3/4 F	Road			n -	e aye	i tir if	. <del></del>		•	Borehole Summar
		. •	Colorado			te Ma	Aicello	,		Project	PERT
			PN98						Location (N)		(E) <u>23874</u> .66
			6800.5		/Auger	ter (inch l			·	Hole Depth (F	Ft) /7
Drilling Date Dr	cover In Method	3 A		Silic te Pa e Dev	0.5 0.5 chip dlock N	in	0:5 t 0:5 t 0:5 t	Sampli	ing Method iid Level/Date	Stick-Up Heig Slot Size Location Sketch	urd
Sample: Depth*		PiD ppm	Sample No.; Interval	W	TELL STRUCTION	GRAPHIC		temarks _			
0 - 2 - 4 - 6 8 io 2 - 14 16 18			10-12' 12-14' 15-17'	Sand Pack	Screen Casing	Sand wygraved fine sandy silt	Typical to well); to sature  Push by resista	grain ang ated).  Somp  mee i  w/gra  1/5  /gran  gand g	unsell color; per gularity; indurati ling to le necreases vel and vel and valel w	some at colles	es, some times.
			pround lovel. Bedle	4-		Voi	fied Rv				

All depths measured from ground level.

Completed By T. Barflett

Verified By \_

All depths measured from ground level.

pleted By Verified By

Verified By

Borehole Summa

MACTEC-ERS

Completed By 7.

pleted By T. Bartlett

round Elev. (Ft.) 6801.3 Bit/Auger Size Zinch o.d. Hole Depth (Ft.) 19.5 Part of Agricultural Policy (Ft.) 6801.42 Diameter (inch i. D.) No. of Completions 1 Stick-Up Height (Ft.) 0.12 No. of Completions 1 Stick-Up Height	ility		<i>N</i>	/A .			Site	Mo	bicello	Project PERT
TOC 690.42 Diameter (Inch. I. D.)  TYPE Vol. (61, 62)  Interval (Ft.)  Stick-Up Height (Fo.)  Stock-Up Height (Fo.					îS	-/	7	<del>.</del>		· · · · · · · · · · · · · · · · · · ·
in Casing pVL 0.5" Interval (Ft.)  In Casing pVL 0.5" O to BA Stock Weight (Ft.)  If Policy of PVL 0.5" O to BA Stock Weight (Ft.)  If Policy of PVL 0.5" IS to BA Stock Weight (Ft.)  If PVL 0.5" IS to BA Stock Weight (Ft.)  If PVL 0.5" IS to BA Stock Weight (Ft.)  In PVL 0.5" IS to BA Stock Weight (Ft.)  In PVL 0.5" IS to BA Stock Weight (Ft.)  In PVL 0.5" IS to BA Stock Weight (Ft.)  In PVL 0.5" IS to BA STOCK WEIGHT (Ft.)  In It Is a single policy of the PVL of the P										Hole Depth (Ft) 19.5
perfend Cap  PVL 0.5"  Better Cap  PVL 0.5"  PVL 0.5"  Better Cap  PVL 0.5"		·		TYPE		Vo	ol. (cf.	. gal)	Interval (Ft.)	Stick-Up Height (Ft) 0.12
d Pack 10-20 2-15 18 to 18.5 t		esing	-	pri		0	.5-11		13.4 to 18.4	
Sampling Method   Sample   Sampling Method   S	np/E	nd Cap	-20 ·	PVC		0	511		18.4 to 18.5	
Padjok No. NA  Sampling Method 2 core borned  The provided 1/8 forestoke  Sampling Method 2 core borned  Fluid Levelipate 16.12 Exc 1/8/16  Padjok No. NA  Remarks 5 min of creek in the  Butth North State of the policy of the p	Sealant		4	entonite	de	ips				
Sampling Method 2' core barret  gate Developed NA  Full Level/Date of 1.2570c 1/9/16  Remarks 5 - 16 - 1.2570c 1/9/16  Remarks 5 - 16 - 1.2570c 1/9/16  Remarks 5 - 16 - 1.2570c 1/9/16  Required Information:  Typical name; Munsell color; percentage sand and gravel; sorting (poor to vell); grain angularity; induration or plasticity; moisture content (moist to saturated).  Easy with a fact to 5' 5' interest to saturated.  Easy with a fact to 5' 5' interest to saturated.  Easy with a fact to 5' 5' interest to 1' 1' 1' 1' 1' 1' 1' 1' 1' 1' 1' 1' 1'	kind	Cover	- Install	ed Y (N)		adio	ck No	<u>-</u> //		
Remarks State of Control of the State of Control of the State of Control of the State of Stat	rilling l	Method		19/98					Samplin	ig Method Z'core barrel
Required Information: Typical name; Munsell color; percentage sand and gravel; sorting (poor to well); grain angularity; induration or plasticity; moisture content (moist to saturated).  Easy when finely & surface the first and the first an			Bar	Hett 1	Vor	the	Tre	VIND	Remarks	S. mth of Creek 118/98
Required Information: Typical name; Munsell color; percentage sand and gravel; sorting (poor to well); grain angularity; induration or plasticity; moisture content (moist to saturated).  Easy when funch to 8' surprished to saturated.  Easy when funch to 8' surprished to saturated.  Easy when funch to 8' surprished to 15' surprished to saturated.  10-11' florder funching at 11' (surel)  10-11' releasered 1' of dry children function for the same of		L.	-				ICTION	GRAPHIC		
Typical name; Munsell color; percentage sand and gravel; sorting (poor to well); grain angularity; induration or plasticity; moisture content (moist to saturated)  2  2  2  3-16 any make, sumple a lifetal  3-16 any make, sumple a l						1	1	200	•	
to wear, grain angularity, induration or plasticity; moisture content (moist to saturated).  Easy when fund to 8' single of the saturated is a first of the saturated in the sat										
Ensymmetry fruck to 8' somegrithment  8-16' encympton a Heater  10-12' therefore pushing a 11' (somet)  10-12' sultry to a somety of and somety to  11-12' sultry to a somety of dry while fromys to  12-14' recovered 1' of dry while fromys to  14-16' recovered 0.8' of dry while fromys to  Sind 55 to discrete cubble to yments  12-18' somety 18-18' somet									to well); grain angu	larity; induration or plasticity; moisture content (moist
8-16 any pick, simple attential  siming of the series of the series  10-12 thereof pushing at 11 (govern)  10-12 sitty to and appel to ables master  12-14 recovered 1 of dry childe brogs to  12-14 recovered 1 of dry childe brogs to  simily gil  14-16 recovered 1 of dry childe brogs to  10-18 since the coulde be yeards  10-18 since the coulde be yeards  10-18 since the sit of the series  10-18 since the sit of the series  11-18 since the sit of the sit of the series  11-18 since the sit of the sit of the series  11-18 since the sit of the sit of the series  11-18 since the sit of the sit of the series  11-18 since the sit of the sit of the series  11-18 since the sit of the sit of the series  11-18 since the sit of the sit of the series  11-18 since the sit of the sit of the series  11-18 since the sit of the sit of the sit of the series  11-18 since the sit of	70 -									hard it si sind ittend
10 - 12 Herder pushing a 11' (g. rel)  10 - 12' Herder pushing a 11' (g. rel)  10 - 12' silty + c soul of get + whiles mass - 12-14' recovered 1' of dry childe brought and  12-14' recovered 0.8' of dry childe brought and  14-11' recovered 1' of dry childe brought and  10 - 18   15' recovery 10 17' saming get / childe  10 - 18   15' recovery 10 17' saming get / childe  11 - 18   18 - 19   Sound of get a grade sto group of depth.  18   18 - 5 1   18 5 to 19.  18   18   18   5   19   5   countles		. 7								
10 10 10 10 10 10 10 10 10 10 10 10 10 1		- 2		_	<u>.</u>			! i	5-Ly , 1+ -	= i must set it - 7.5-10'
10 10 10 10 10 10 10 10 10 10 10 10 10 1		-4			_			:		
12-14 recovered " if dry while from the same gold of the same same gold of the same same same same same same same sam		•						14.	10-11 11 5m	Exist mont wet set
14-11' recovered 0.8' of dry calles gol with Sink 5s + dion to calle to yments  12-18 15' recovery 16-17' saily gol / albles  11-18 15' recovery 16-17' saily gol / albles  11-18 15-18 saily sol outed  11-18 18-19.5 New thereof shall  18-19.5 New thereof shall  18-19.5 New thereof shall  18 18-5-19.5 New thereof shall  18 18-5-19.5 New thereof shall  18 18-5-19.5 New thereof shall  18 18 19-19.5 New thereof shall  19 19-19.		-6		-				45	11-12' silly +	-c and ofgot + orthes must-u
10 Sink 5s + dior to cobble to ments  Matrix is muist  11-18 15 receivery 16-17' saily gol / abbles  11-18 18-18 sail side of the libbs  11-18 18-19 Show thereof shale  18 -19 5 New thereof shale					, i	a t				red of dry whole trays to
10   Sint 35 + dier to cobble to yments  Mutrix is muist  10-18 /5 receiving 10-17' saily got /c. 46/c.  11-18 /5 receiving 10-17' saily got /c. 46/c.  11-18 /5 saily solve started 5+9.  18 -19 S New thereof shall  18 S New thereo		-8	1		4	7	4			- 105( ( 1 111 / 1
12   12   15 receivery 16-17 Sanity gol /c. 46/cs  18-18-18-19-5 wentered 5+9.  18 - 19-19-5 Wenthered shall  18 - 19-19-5   18-5 to 19.  18 - 19-19-5   18-5 to 19.  18 - 19-19-5   19-19		-10			3	1	7		Sind St L	land and be to the first with which
12   12   15 receivery 16-17 Sanity gol /c. 46/cs  18-18-18-19-5 wentered 5+9.  18 - 19-19-5 Wenthered shall  18 - 19-19-5   18-5 to 19.  18 - 19-19-5   18-5 to 19.  18 - 19-19-5   19-19		10			9		3		Matrix is me	ist.
18 - 18 - 18 - 18 - 18 - 18 - 18 - 18 -		12	-		14	ļ	\ <u>\</u>		16-18 1.5' re	every 16-17' sanity got / 1.46/cs
18 - 19.5 - 19.5 Wenthered shall  18.5 - 19.5 Wenthered shall  18 - 19.5 - 19.5 Wenthered shall  18 -				ļ		1		7	mosst. 17-1	8 same; sufferented
18 - 19/18   18 - 19   18   19   19   18   19   19   18   19   18   19   19		14	1					64	10-18.5 5	Auraca 5+9.
18 18 st. 19-19 5. combles			4			4		13	18.5-19.5	Wenthered shale
18 firm s/. wasst 19-195. combles		طا طا	V 7	19/98		4	+	178	yellow ola	regrides to gray us depres.
		10				V	`	N 3	<i>7</i> · ·	
20 TD MASTER 18.5		1p			-	=	-	Ichare		
		20		70-				Mrac.	505 50	218.5

\_\_\_\_ Verified By \_\_

Facility N/A	Site	Montreello	Project PERT
Boring/Well No. PW 9	8-18	· ·	Location (N) 10/18.72 (E) 23953.77
Ground Elev. (Ft.) <u>680 4</u>	Diameter (inc	* :	Hole Depth (Ft) 23.5 No. of Completions
TYPE		Interval (Ft to	
· · · · · · · · · · · · · · · · · · ·	VC.	15.5 to 20.5	
	PVL	20.5 10 20.	
Sand Pack 10-20 20/40	Salica Sand	0.5 to 20.0	
Bealant Bent,	- /	0 to 0.5	-
Grout		<del></del> +o	
Locking Cover Installed Y	N Padlock No	)/A	
Orilling Method Geopra		Samp	ling Method Zft core barrel
Date Drilled 6/8/98	Date Developed	/A- FI	uid Level/Date - 45' South of PW98-17
Sampler(s) Butlett	North Trevino	Remarks	18.8' BTOL 6/19/98
Depth* Blows/ PID Sample (FT) 6" ppm Inter-		PHIC DESCRIPTION	
0		Required Inforr Typical name; M to well); grain an to saturated).	mation: lunsell color; percentage sand and gravel; sorting (poor igularity; induration or plasticity; moisture content (moist
0-10"		Direct bush to	10' Wo sampling. Easy push (sendy sitt)
10-12			
10-12	-	2 recovery/das	K red/brown sandy silt, moist N. moist
1 1 - 11	. 1 1 1	soft, easy fush	
12-14'		Sandy silt soft,	moist to 13.
>T   T	7 1 1 7 3		sand of gravel fie.
			g silt, v. moist/wet, soft.
+   + , ,	.		
14-16	1 . 3 . 1 . 3	Sandy set V. 1	noist/Soff easy fush.
10-18	1 2 2 3 3	Recovered 1 of	- sity sand w/some f. gravel, moist, seft
10+	10 0 0 D	\	1 190000 190000000000000000000000000000
10-70		( PM)	
+ 1000	[ ] [ ]	No recovery. E	Easy push
70-77	1 / San	d 20 = 20 5 call	by send +941. wet
		20.5-21 60.1	1/9 ravel/colbles some fines, saturated
15+ +	+     +		
		a a clay	/weathered mudstone, yellow, soft,
+ 1 -1	J. Sur	WEO'.	as well down int
25-53	.5 3	22-22.2 cla	y . soft, yellow/gray , moist
6/19/98	(3)	22.2-23.5	Audstone shale, goay, by, tirmes.
72	-   V		
	Sand -		(1
		7	
+   +	Mulsto	re	
TD		1	
25			
All depths measured from ground is	val.		
ompleted By T. Bar	. 1 11	Varieties d. D.	
ompleted by	1104 V	erified By	· ·

Borehole Summary

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# Appendix B

**Borehole and Completion Logs, 1992 Field Program** 

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#### MONITORING WELL COMPLETION LOG 88-85 Project: Monticello Mill Tailings Site North Coordinate (ft.): 10.336.2 Date Orilled: 09/30/88 East Coordinate (ft.): 23.982.7 Location: Monticello, Utah Drilling Method: Hollow-Stem Auger Site: Downgradient, just east of East Tailings Pile Ground Elevation (ft. MSL): 6797.1 Sampling Method: Split Barrel Total Depth (ft.): 12.5 Measuring Point Elev. (ft.): 6797.6 Development Date: Unknown Auger Head Size (in.): Unknown Auger Stem Size (in.): Unknown Water Level (ft. BGL): Unknown WELL INSTALLATION INTERVAL (fL) BIT SIZES (in.) Blank Casing: 2.0 in. SCH 40 PVC +0.5 to 6.5 Not Applicable Screen: 2.0 in. SCH 40 PVC 6.5 to 11.5 Slot Size: 0.02 in. End Cap: 2.0 in. SCH 40 PVC 11.5 to 12.0 SURFACE CASING (fL) Grout: Unknown 0.0 to 6.5 Protective Steel from +L6 to LO Sealant: NA Sand Pack (U): Unknown: 6.5 to 12.5 Sand Pack (L): NA Comments: Locking cap. Well Completion Graphic Log Blows/8-in Ē Diagram Sample No. Description Logged By: M. Kautsky SANDY SILT, ML, brown (7.5YR 4/2), dry to slightly moist, 18-21 -9.0 SANDY GRAVEL, GP, brown (7.5YR 4/2); coarse grained, 50 dense, saturated: 10-10074" 12.5 DAKOTA SANDSTONE. Total depth drilled was 12.5 feet. 15-20-8885.LOG RUST Geotech Inc. Page 1 of 1 Date Drawn: 03/02/1994

MONITORIN	G WELL COMPLE	TION LOG 92-07
Project: Monticello Mil Tailings Site Location: Monticello, Utah Site: Downgradient, just east of East Tailings P Total Depth (ft.): 21:33 Auger Stem Size (in.): 4.5 ID X 7.625 OD	North Coordinate (ft.): East Coordinate (ft.): Be Ground Elevation (ft. MSL): Measuring Point Elev. (ft.): Auger Head Size (in.):	
MELL INSTALLATION  Blank Casing: 2.0 in. Trillok Sch 40 PVC  Screen: 2.0 in. Trillok Sch 40 PVC  Slot Size: 0.010 in.	INTERVAL (fL) +2.25 to 15.3 15.3 to 20.3	BIT SIZES (in.) Not Applicable
End Cap: 2.0 in. Trilok Sch 40 PVC Grout: Envirophyg Sealant: 1/4 in. Envirophyg Pellets Sand Pack (U): \$20-40 Silica Sand Sand Pack (L): \$10-20 Silica Sand	20.3 to 20.7 2:0 to 9.5 9.5 to 12.6 12.6 to 13.0 13.0 to 21.3	SURFACE CASING (ft.) 4.0 in. Protective Steel from +2.57 to 2.43 Cement Pad from +0.37 to 2:0 Comments: CME-75 Drill Rig
Semple Int. Semple	Graphic	Description
5/6 7/9 7/11: 13/12 5- 9/10 9/9 7/8 9/11 7/6 6/6 3/5 10/10 3/5 8/21 13/13 8/10 18/40 refusal 28/28 50-5 32/50-5		SANDY SILT/SILTY SAND, dark brown (7.5YR 4/3), dry, stiff, roots throughout, moderate HCI reaction.  2.0 Not as stiff as above, firm, 5% caliche on fractures, strong reaction to HCL, dry.  -5.0 Same as above, dark brown (7.5YR 4/3).  -6.0 Dark brown (7.5YR 3/2), stiff, 2% caliche, 1% black oxidized organic material to 1/4 in., slightly moist.  -Little caliche below 9.0 feet, moderate HCL reaction down to 9.8 feet then no HCL reaction, moist at 9.6 feet.  -10.0 SILTY SAND/SANDY SILT, dark brown, very fine-grained sand, no caliche.
RUST Geotech Inc.	<u> </u> -	File: 9207.log Date Drawn: 02/04/1994 Page 1 of 1

#### MONITORING WELL COMPLETION LOG 92-11 North Coordinate (ft.): Project: Monticello Mil Tailings Site 10.618.07 Date Drilled: 10/01/92 Location: Monticello, Utah East Coordinate (fL): 23.652.29 Drilling Method: Hollow-Stem Auger Downgradient, just east of East tailings Pile Ground Elevation (ft. MSL): (6806.5) ~6813 Sampling Method: Split Barrel, 3.0 in. X 24 in. Measuring Point Elev. (fL): (6808.93) 6813.73 Total Depth (ft.): 14.2 Development Date: 10/09/92 - 10/20/92 Auger Head Size (in.): 8.0 Auger Stem Size (in.): 4.5 ID X 7.625 OD Water Level (ft. BGL): 12.33, 10/17/92 WELL INSTALLATION INTERVAL (fL) BIT SIZES (in.) Blank Casing: 2.0 in. TriLok SCH 40 PVC +2.43 to 9.53 Not Applicable pre 12/93 Screen: 2.0 in. TriLok SCH 40 PVC 9.53 to 13.88 0.010 in. Slot Size: End Cap: 2.0 in. Trilok SCH 40 PVC 13.88 to 14.18 SURFACE CASING: (ft.) Grout Cement 0.0 to 4.0 4.0 in. Protective Steel from +2.7 to 2.3 Sealant: 1/4 in Enviroping Pellets 4.0 to 7.0 Cement Pad from +0.37 to 4.0 Sand Pack (U): #10-20 Silica Sand 7.0 to 14.18 Connents: CME-75 Drill Rig Sand Pack (L): NA Well Completion Graphic Log Diagram Sample No. Description Logged By: D. Traub :2/16 seil SILT, sandy, brown (7.5YR 5/2), dry, no caliche or pebbles, moderate reaction to HCL. 10/14 samo:es 2/3 2.0 SILT, with very fine-grained sand, stiff, dry, slightly clayey, 4/6 seved fine-to medium-grained sand content increasing. 678 4.6 SAND, silty, dark brown (7.5YR 4/2). 779 6.0 SILT, sandy, dark brown, firm, moist, grades into a silty, -2/12 medium-grained sand. 10% pebbles to 3/4 in. from 7.8 to 8.0 feet. Minor reaction to HCE throughout. 12/14 9720 8.0 GRAVEL, sandy, slightly silty, iron stained, various colors depending on pebble type (igneous or sandstone), fractured 22/26 igneous and sandstone peobles to 2 in. with 90% less than 1/4 16/26 in. Moist to 8.5 feet, then saturated. Fractured, subrounded to subangular, igneous pebbles to 2 in., 32/38 silty and sandy to 11.0 feet, then little silt from 11.0 to 12.0 feet 0/6 GRAVEL, sandy, slightly silty, medium-to coarse-grained; slightly 9/25 silty, subrounded to subangular igneous pebbles, 70% gravel, 25/0" 25% sand, 5% silt. 15-14.1 DAKOTA SANDSTONE, SILTSTONE, dark gray, fragments on center bit, drilling hard, auger refusal. LTotal depth drilled was 14.2 feet. 9211.log RUST Geotech Inc. Page 1 of 1 Date Drawn: 02/07/1994

#### MONITORING WELL COMPLETION LOG P92-08

Project: Monticello Mill Tailings Site

Location: Monticello, Utah

Site: Downgradient, just east of Milsite

Total Depth (ft.): 16.0

Auger Stem Size (in.): 4.25 ID X 7.625 00

WELL INSTALLATION

Screen:

Blank Casing: 2.0 in. Trilok SCH 40 PVC 2.0 in. Trilok SCH 40 PVC

Slot Size:

0.010 in.

End Cap: 2.0 in. Trilok SCH 40 PVC

Enviroplug

Grout:

Sealant: 1/4 in. Enviroplug Pellets

Sand Pack (U): #20-40 Silica Sand

Sand Pack (L): NA

North Coordinate (ft.):

Auger Head Size (in.):

INTERVAL (fL)

+2.46 to 12.0

12.0 to 14.5

14.5 to 14.85

2.0 to 10.5

10.5 to 11.5

11.5 to 16.0

East Coordinate (ft.): 23,940.9

Ground Elevation (ft. MSL): 6804.9 Measuring Point Elev. (ft.): 6807.4

10,496,9

Date Drilled:

10/04/92

Drilling Method: Hollow-Stem Auger

Sampling Method: Split Barrel, 3.0 in, X 24 in.

Development Date: NA

Water Level (ft. BGL): Dry, 10/04/92

BIT SIZES (in.)

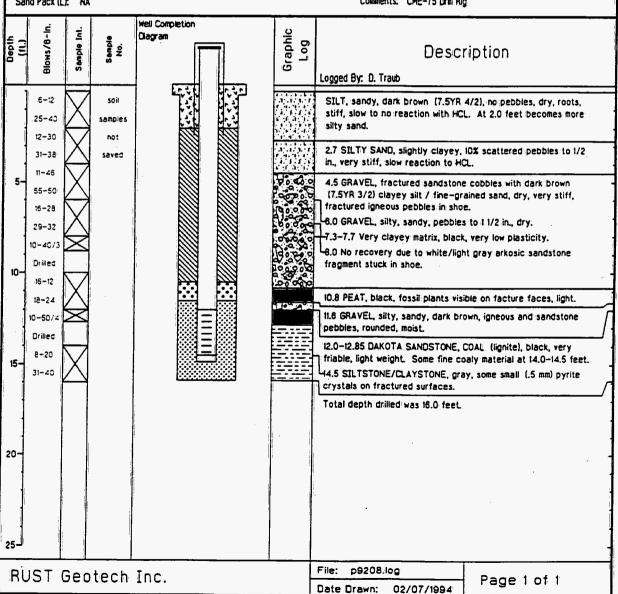
Not Applicable

SURFACE CASING (ft)

4.0 in. Protective Steel from +2.78 to 2.22

Cement Pad from +0.43 to 2.0

Comments: CME-75 Drill Rig



Project: Monticello Mill Tallings Site Location: Monticello, Utah

Site: Downgradient, just east of Millsite

Total Depth (ft.): 30.5

Auger Stem Size (in.): 4.25 ID X 7.625 00

North Coordinate (fL): 10,044.4 East Coordinate (ft.): 23,963.3 Ground Elevation (ft. MSL): 6811.4 Auger Head Size (in.): 0.8

Date Orilled: 10/03/92 Drilling Method: Hollow-Stem Auger Sampling Method: Split Barrel, 3.0 in. X 24 in. Water Level (ft. BGL): -27.0, 10/03/92

Remarks:

<u></u>		,			
Depth (11.)	Blows/8-in.	Sample Int.	Semple No.	Graphic Log	Description
					Logged By: D. Traub
	4-5	M	soit		SILT, sandy, dark brown (7.5YR 4/3), slightly clayey, fine—grained sand, dry, strong FCL reaction, roots and minor caliche increasing to 2.0 feet.
	<b>8−</b> 9	$\square$	samples		-2.0 Clay content slightly higher than 0-2 foot interval, caliche increases to 3% and is in fractures
.	4-7	M	not		and filling in worm holes.
	5-3	V V	savec		A D CTI TV CAND/CANDV CTI T alighbly along the bar - /7 EVD 4/2) and 6-2
5-	5-7	$\bigvee$			-4.0 SILTY SAND/SANDY SILT, slightly clayey, dark brown (7.5YR 4/3), very fine-graned sand. 4.0-6.0 feet, moisture increases and scattered gray siltstone pebbles to 1/2 in.
	ε-7	/			
	4-6				-6.0 Same, moist, strong reaction to HCL. 1.1 foot of sample recovered (compressed).
1	€-5	$ /\backslash $	;		
	2-3				-8.0 SANDY SILT/SAND (very fine grained), minor clay, dark brown, low plasticity, no callone, strong reaction to HCL, moist, siltstone fragments and pebbles to 1/2 in. from 9.0-10:0 teet.
	4-5	$ \Delta $			
10-	3-5	M			-0.0 SILT, sandy, little clay, very fine-grained sand, 20% dark gray siltstone fragments, very strong HCl reaction, no caliche. I.I foot of sample recovered.
	5-6	$ \triangle $			
	1-4				H2.0 SANDY SILT/SILTY SAND, dark brown (7.5YR 5/4), softer and more saturated in sandy zones. 1.4 foot of sample recovered.
	5-5	$ /\backslash $		· a· . i . s . r r . 4 , i . s . i	
15-	2-2	M			-14.0 Saturated in sandy zones, very moist in sitty zones.
13-	5-6	$ \Lambda $			=15.6 Very silty with abundant siltstone fragments horizontally bedded.
1		$\mathbb{H}$	j		746.0 SANDY SILT/SILTY SAND, matrix approximately 70% around siltstone fragments. (cark gray).
	6-9 18-:4	X			several fractured light brown sandstone fragments to 3 in., fine-grained sand, moist, fra.
	€-3				
	e5	ΔI			
20-		$\vdash$			Slightly more clay at 19.7 feet. (for 0.1 foot interval), then silt, very fine-grained sand.
	5-6	V			420.0 SANDY SILT/SILTY SAND, dark brown (7.5YR 5/4), very minor clay, several ver, hard light gray siltstone fragments, wet, firm.
	7-8				,
	2-3	$\bigvee$			—22.0 Same, slightly diayey (low plasticity) in several 0.1 foot intervals.
	4-6				
25_	5-9	X	ļ		24.3 SAND, dark brown (to 24.6 feet), fine-grained sand, no silt or clay, soft, wet.
					· ·
Rl	JST	Geo	tech	Inc.	Page 1 of 2
					Date Drawn: 02/04/1994

					SOIL BORING LOG SB 92-06
Depth (Ft.)	Blows/6-In.	Sample Int.	Sample No.	Graphic Log	Description
30-	13-20 11-15 32-26 10-14 11-12 5-21 33/5			\$ 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	24.8 SILTY SAND/SANDY SILT, 30% subrounded siltstone and sandstone peoples to 3/4 in., wet.  26.0 GRAVEL ??, no recovery except for a 3.0 in igneous rock fragment and several subrounded to subangular igneous peobles to 1 1/2 in.  28.0 GRAVEL, sandy, saturated, 80% of peobles (igneous/sandstone) 1/2 in., silty from 29.5-30.0 feet. Very wet/saturated gravels above bedrock.
35-					
40					
45-					
RU	JST	Geo	otech	Inc.	File: SB9206.log  Date Drawn: 02/04/1994  Page 2 of 2

Project: Monticello Mill Tailings Site Location: Monticello, Utah

Site: Downgradient, just east of Milsite

Total Depth (ft.): 14.0

Auger Stem Size (in.): 4.25 ID X.7.625

North Coordinate (fL): East Coordinate (ft.):

Auger Head Size (in.):

10,337.6 23,928.6 Ground Elevation (ft. MSL): 6,797.8

10/04/92 Date Drilled:

Draing Method: Hollow-Stem Auger Sampling Method: Split Barrel, 3.0 in. X 24 in.

Water Level (ft. BGL): -7.4, 10/04/92

Remarks:

					·
Depth (11.)	Blows/8=In.	Semple Int.	Semple No.	Graphic Log	Description Logged By: D. Traub
10-	12-14 17-8 4-5 6-6 3-3 5-6 8-9 3-7 5-14 22-19 50/3" 50UNCED 3-6 18-26		soil samples: not saved	\$ 600 \$ 600 \$ 600 \$ 600	Logged By: D. Traub  GRAVEL, silty, sandy, dark brown, igneous peobles, some (C.2 foot) brown sandy silt on the surface.  —7.7 SANDY SILT, dark brown, very fine-grained sand, moist, stiff, igneous gravel may be fill finaterial, not the same type of gravel as in the creek bed.  —2.0 SANDY SILT/SILTY SAND, dark brown (7.5YR 3.2), slightly clayey in thin 1/2 in. layers, very fine-grained sand, moist, firm, no HCL reaction except for 2% calicne from 2.0-3.0 feet, minor calicne from 3.0-4.0 feet.  —4.0 SANDY SILT/SILTY SAND, dark brown, very fine-grained sand with minor low plasticity clay, firm, wet, no pebbles or caliche present.  —5.3 GRAVEL, sandy, silty, with 60% pebbles to 3/4 in., wet, scattered pebbles to 2 in., subrounced to subangular.  —7.4 SAND, very silty, dark gray, 20 % pebbles to 11/2 in., seturated.  —6.0 GRAVEL, silty, sandy, grading from very fine-grained sand to pebbles 3 in. across, igneous and sandstone pebbles, subrounced to subangular.  —6.0 OR or recovery, sampler refused, large boulder.  —6.10 GRAVEL, sandy, well graded, saturated to 13.2 feet.  —6.20 GRAVEL, sandy, well graded, saturated to 13.2 feet.
25-J Rl	JST	Geo	tech	Inc.	File: \$89207.log  Date Drawn: 02/04/1994  Page 1 of 1

Project: Monticello Mili Tallings Site

Location: Monticello, Utah

Site: Downgradient, just east of Millsite

Total Depth (ft.): 30.9

Auger Stem Size (in.): 4.25 ID X 7.625 OD

North Coordinate (ft.): East Coordinate (ft.): 9959.7

23,899.0

Auger Head Size (in.): 8.0

Ground Elevation (ft. MSL): 6822.5

Date Drilled: 10/15/92

Drilling Method: Hollow-Stem Auger Sampling Method: Split Barrel, 3.0 in. X 24 in.

Water Level (ft. BGL): NA

Remarks:

Depth (rt.)	Blows/8-fn.	Semple Int.	Semple No.	Graphic Log	Description
	ĕ	S		9	Logged By: D. Traub
	3-8	$\square$	soil		SAND, silty, dark brown (7.5YR 4/3), fine grained, dry, slow to moderate HCL reaction, few peobles, minor caliche.
	9-9	M	samples		
	7-10	$\bigvee$	net		−2.0 Same, brown to dark brown, dry, small roots, caliche on fractures and root/insect/worm holes.
	10-9		saved		—4.0 Same, stronger HCL reaction.
5-	7-ti				· · · ·
	12-16				-6.0 Same, abundant caliche, several small peobles (sandstone, igneous, and claystone to 3/4 in.
	8-9 13-15	X			[2-3%]), very strong HCL reaction.
	13-14	$\mathbb{H}$			−8.3 SAND, light gray (10YR 6/1), claystone fragments present, 30% sand, strong HCL reaction.
	14-16	X			-9.1 SAND, silty, brown (7.5YR 5/4), fine grained, dry, 5% pebbles at 1/2 in., minor caliche, strong HCL reaction.
10-	10-11				740.0 SAND, silty, light brown (7.5YR 6/4), fine grained, scattered siltstone/claystone pebbles, very strong HCL reaction.
	13-15	$\triangle$			=12.0 No sample collected, sampler broke and drillers had to overdrill to 13.5 feet to retrieve.
	Drilled				-2.0 NO Sample Conected, Sampler broke and dimers had to overdrik to 15.5 lest to retrieve.
	Drilled				-4.0 SAND, silty to slightly silty, fine grained, 5% fractured claystone fragments to 3/4 in., very
15-	9-15	X			strong HCL reaction. Very little silt from 14.7 to 15.2 feet.
	16-16	$\left( \cdot \right)$			
	11-17	X		V. 60.0	⊣6.7 Claystone fragments, angular, 4C%.
1	14-17				→8.4 SAND, brown (7.5YR 5/4), 20% coarse grained, slightly moist, moderate HCL reaction
	21-29	X			(18.0-18.4 feet), slight HCL reaction (18.4-20.0 feet), very firm, color grades from light brown to brown over 0.2 foot interval at 18.3 feet.
0-	11-19	$\bigvee$			F20.0 SAND, silty, clayey, dark brown (7.5YR 4/4), very fine to fine grained, no HCL reaction, white calcareous material (3%) on fracture surfaces (strong HCL reaction), scattered gypsum
	26-34				crystals at 21.5 feet, subrounded, 1/2 in. igneous peobles at 20.3 feet.  —22.0 SAND, very silty, clayey, strong brown (7.5YR4/6), moist, low plasticity, slightly less
	17-21	$\bigvee$			calcareous/caliche white material on fractures than at 20.0-22.0 feet, very stiff.
	30-40				24.4.5.110 - (1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.
25_	12-14	$\preceq$		3°.1.31	-24.4 SAND, sitty, brown (10YR 5/3), dry to slightly moist. I in.
	. С. Т	_		_	File: SB9208.log

RUST Geotech Inc.

File: SB9208.log

Date Drawn: 02/07/1994

Page 1 of 2

	SOIL BORING LOG SB 92-08								
Depth (Ft.)	Blows/8-In.	Sample Int.	Sample No.	Graphic Log		Des	cription		
30-	16-24 15-34 50/5" 33-50/4			30000000000000000000000000000000000000	-25.8 1 in: layer of subrounded feet, then decrease in pebble 27.2 GRAVEL ??, Sampler refusioneded to angular.  -28.9 Sampler refusal, igneous in tip of sampler, very hard dri	s to predominate	ely sand, minor HCL r	neous peobles to 3.0	in.,
	50/5**			0000	730.5 DAKOTA SANDSTONE, SA Totalidepth drilled was 30.9 fe		very hard drilling: ()	bit teeth were Samag	ped).
35-								:	
40-									
45-									
50									
RL	RUST Geotech Inc.					File: \$8920 Date Drawn:		Page 2 of	2

Project: Monticello Mill Tallings Site

Location: Monticello, Utah
Site: Downgradient, just east of Millsite

Total Depth (ft.): 14.0

Auger Stem Size (in.): 4.25 ID X 7.625 00

North Coordinate (ft.): 10,438.2 East Coordinate (ft.): 23,931.9 Ground Elevation (ft. MSL): 6798.7 Auger Head Size (in.): 8.0

Oate Orilled: 10/04/92

Orilling Method: Hollow-Stem Auger

Sampling Method: Split Barrel, 3:0 in. X 24 in.

Water Level (ft. BGL): 6.0, 10/04/92

Remarks:

Depth (11.)	Blows/8-In.	Sample Inf.	Semple No.	Graphic	Description Logged By: D. Traub	
1	i			11.11.11		
	3-6 8-11	X	soil samples		SANDY SILT/SILTY SAND, slightly clayey, dark brown-(7.5YR 4/2), very low plasticity, dry, stiff, strong HCL reaction.	
			. sompics	1	14 1-2.1 SAND, slightly silty, very fine grained, slightly moist, some roots, soft. At 2.7-2.9 feet sendy,	
	7~9	X	not		slightly clayey, dark brown silt. More sand in sampler shoe. Elevated radiation levels in this zone.	
	7-4 2-2	$\square$	saved		4.0 SAND, very silty iin 0.3 foot intervals, dark brown, moist. At 5.4 feet, 0.1 foot (12 in.) layer of wood (doesn't look like roots). Selow to 6.0 feet, very silty sand, slightly clayey, dark brown, low	
5-		X			plasticity. Several subrounded to subangular igneous peobles in sampler shoe to 1.5 in.	
	3-5	$oxed{oxed}$				
	3-8. 9-12	X		V 6 63 0 0 0 0 0 0 0 0	6.0 GRAVEL, sandy, dark brown to 8.0 feet, very minor silt or clay, igneous pebbles, subrounded to subangular to 2 in., 75% of material is 1/2 in. or smaller in diameter, saturated.	
	a-7	$\mathbb{N}A$		0000		
	12-20	X		1 1 1	9.2 SAND, silty, dark gray, with a few scattered pebbles.	
10-	18-38-1		i	V: 60	10.0 GRAVEL, sandy, dark brown, with fractured light gray sandstone and igneous (diorite)	
		X		9070	pebbles/cobbles to 3 in., saturated, siltier at 12.0 feet.	
	28-29			19000	<b>o</b>	
	3-10	$  \bigvee  $				
i	11-8	$ \Delta $	į	0000	·	
	İ				713.7 DAKOTA SANDSTONE, CLAYSTONE, dark gray. At 14.0 feet, iron staining (rust) on. fractures.	
15-					Total depth drilled was 14.0 feet.	
20-				,		
-						
25						
RI	JST	File: S89212.log Page 1 of 1				
1			Date Drawn: 02/04/1994			

Project: Monticello Mill Tailings Site

Location: Monticello, Utah

Site: Downgradient, just east of Millsite

Total Depth (ft.): 21.25

Auger Stem Size (in.): 4.25 ID X 7.625 00

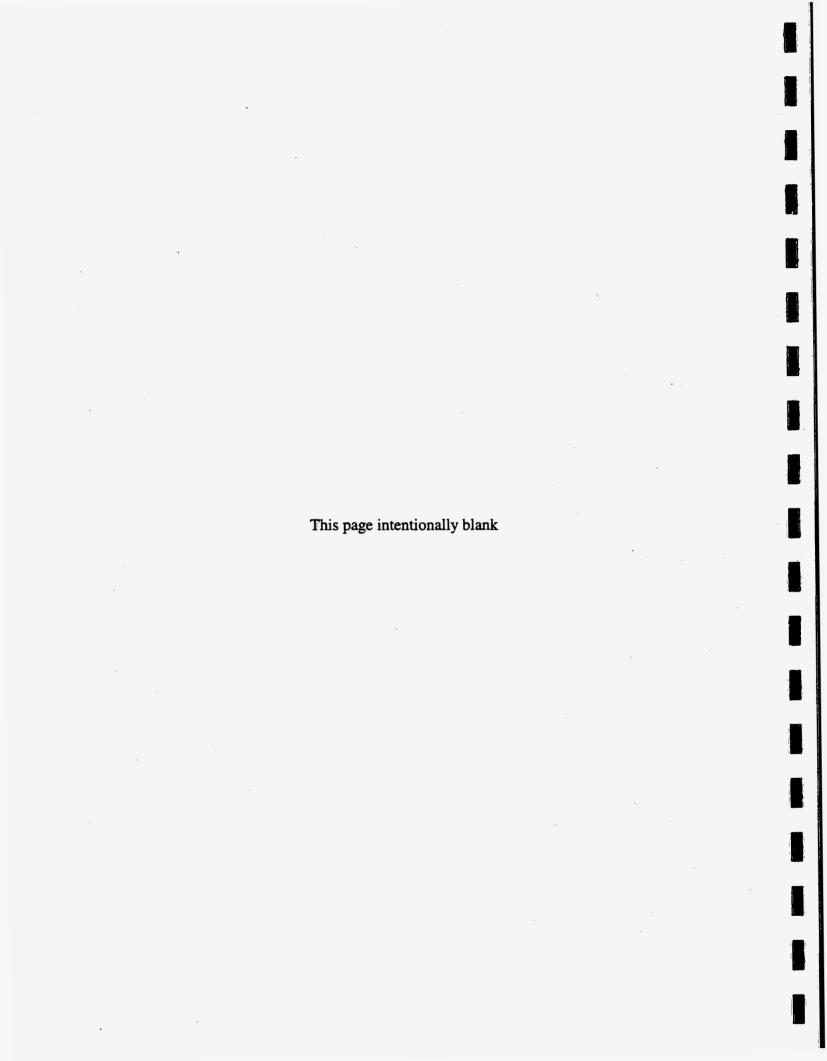
North Coordinate (ft.): 10,110.2
East Coordinate (ft.): 24,005.2
Ground Elevation (ft. MSL): 6802.5
Auger Head Size (in.): 8.0

Date Orilled: 10/03/92

Drilling Method: Hollow-Stem Auger
Sampling Method: Split Barrel, 3.0 in. X 24 in.
Water Level (ft. BGL): 17.2, 10/03/92

Remarks:

		,							
Depth (11.)	Blows/8-In.	Semple Int.	Sample No.	Graphic Log	Description Logged By: D. Traub				
1				1111111	CUTY CANDICANDY STIT AND AND AND AND AND AND AND AND AND AND				
	5-7 8-11	X	soil samples		SILTY SAND/SANDY SILT, stiff, dark brown (7.5YR 4/3), very fine-grained sand, slightly moist, stiff, slight HCL reaction near the ground surface, stronger reaction at 2.0 feet, no pebbles or caliche. 1.3 feet of sample recovered (compressed).				
	5-7	M	nat		72.0 Same, caliche (minor) at 2.0 feet, increases to 5-7% at 4.0 feet, very strong reaction to HCL throughout. At 3.2 feet grades to a darker brown (7.5YR 3/2), very stiff, caliche in				
1	9-10	$ \Delta $	saved		rootholes/fractures.				
_	8-8	$\forall$			—4.0 SILT, sancy, slightly clayey to 5.5 feet, dark brown. 1.0 foot of sample recovered (compressed).				
. 5-	8-9				-5.5 Gradual color change to brown (7.5YR 4/2), 3% scattered pebbles to 1/5 in., 10% caliche on rootholes, slightly moist, stiff.				
	3-7 7-8	X			6.4 SAND, silty, dark brown (7.5YR 4/3), softer than above, but firm. Soft at 7.8-8.0 feet, very fine-to fine-grained sand, 5% blebs of light gray silt to 1/2 in. from 7.0-8.0 feet. 1.5 feet of				
	3-3	3			-sample recoverd.  7-8.0 Same, dark brown, very silty, slightly clayey, low plasticity, fine-grained sand. Some layers  (separation of layers not defined) consist of more silt than sand, moist, strong HCL reaction. 1.7				
10-	4-6	VV			feet of sample recovered.				
ו"	2-2	$\sqrt{A}$			740.0 More silt than sand, saturated from 10.4-10.8 feet.				
1	3-5	IXI		<u> </u>	10.8 CLAYEY SILT, slightly sandy, cark brown [7.5YR 4/3], low plasticity, very moist, stiff.				
1	0+2	$\forall$			→2.0 Same, 20% very fine-grained sand, low plasticity, no HCL reaction. At 13.8 feet, more sand (fine grained) than silt, dark brown, wet, sand layers are more saturated.				
15-	3-5 2-4	$\bigcirc$			H4.0 CLAYEY SILT to SILTY CLAY, cark brown (7.5YR 4/3), very moist. At 14.8, 1.0 in. layer with 20% subrounded igneous and siltstone pebbles to 1/2 in.				
	6-6 2-10								
	21-34 :8-25	$\bigcap$		40.00°	17.2 GRAVEL, sandy, grayish brown, igneous and sandstone pebbies to 3.0 in., 60% of pebbles are 1/2 in. or less, fine—to coarse—grained sand, saturated, 5% black oxidized material.				
20-	22-46	A			-20.0 SANDY GRAVEL, igneous and sendstone pebbles, poorly graded (madium-grained sand to -1/2 in, pebbles).				
+		$\triangle$							
	50/3"		•	. 721.0 DAKOTA SANDSTONE, CLAYSTONE, cark gray, some iron staining.					
25					Total cepth drilled was 21.25 feet.				
5": 00000									
Part of the control o					File: SB9215.log Page 1 of 1				
Date Drawn: 02/04/1994									



# Appendix C

Hydrographs for wells 88–85, 92–11, 92–07, and P92–08

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